# Commissioning of a compact multibend achromat lattice NanoTerasu: A new 3 GeV synchrotron radiation facility

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(Received 24 June 2024; accepted 9 January 2025; published 14 February 2025)

NanoTerasu, a new 3 GeV synchrotron light source in Japan, began user operation in April 2024. It provides high-brilliance soft to tender x-rays and covers a wide spectral range from ultraviolet to tender x-rays. Its compact storage ring with a circumference of 349 m is based on a four-bend achromat lattice to provide two straight sections in each cell for insertion devices with a natural horizontal emittance of 1.14 nm rad, which is small enough for soft x-rays users. The NanoTerasu accelerator incorporates several innovative technologies, including a full-energy injector C-band linear accelerator with a length of 110 m, an in-vacuum off-axis injection system, a four-bend achromat with B-Q combined bending magnets, and a TM020-mode accelerating cavity with built-in higher-order-mode dampers in the storage ring. This paper presents the accelerator machine commissioning over a half-year period and our model-consistent ring optics correction. The first user operation with a stored beam current of 160 mA is also reported. We summarize the storage ring parameters obtained from the commissioning. This is helpful for estimating the effective optical properties of synchrotron radiation at NanoTerasu.

DOI: 10.1103/PhysRevAccelBeams.28.020701

#### I. INTRODUCTION

NanoTerasu is a new 3 GeV synchrotron light source constructed on a green field site in Sendai, Japan. The purpose of this facility is to provide high-brilliance soft and tender x-rays and to cover a wide spectral range from ultraviolet to tender x-rays, using a compact storage ring with a circumference of 349 m as a complementary partner to SPring-8 [1], which mainly covers hard x-rays and is one of the world's most powerful synchrotron radiation facilities. The target brilliance of NanoTerasu is  $\mathcal{O}(10^{21})$  photons/s/mm<sup>2</sup>/mrad<sup>2</sup>/0.1% bandwidth with a coherence ratio 8.1% [2] (3.4% [3]) for photon energies of 1-3 keV.

The designed natural horizontal emittance is 1.14 nm rad with a nominal stored current of 400 mA, and a four-bend achromat lattice is used in the NanoTerasu compact storage ring to meet the electron beam specification. The fourthgeneration synchrotron light sources based on the multibend achromat lattice proposed in 1993 [4] have been in service at MAX-IV since 2016 [5], ESRF-Extremely Brilliant Source since 2020 [6], and Sirius since 2021 [7], and many others are under construction or planned [8–10]. NanoTerasu started user operation in April 2024 as the world's fourth multibend achromat lattice light source.

A schematic of NanoTerasu is shown in Fig. 1. The light source can provide a maximum of 28 insertion device beamlines, although it will provide 10 beamlines in the initial user operation phase. Two beamlines are multipole wiggler (MPW) beamlines, and the others consist of two in-vacuum, one twin-helical, and five APPLE-II undulator

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beamlines. Various beamline designs have been proposed and are being constructed [11–14]. Moreover, the NanoTerasu facility has an upgrade plan to extend the linear accelerator beamlines and serve as a soft x-ray freeelectron laser in the future [15].

In this paper, Sec. II briefly describes the accelerator design, and Sec. III describes the efficient completion of the NanoTerasu accelerator machine commissioning, in which model-consistent storage ring optics and a 200 mA stored beam were obtained within half a year. We also report the first user service time operation in Sec. IV.

## II. ACCELERATOR DESIGN

The NanoTerasu accelerator consists of a 3 GeV linear accelerator as an injector, a beam transport line, and a storage ring. The linear accelerator has a short length of

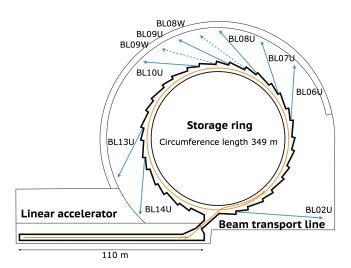


FIG. 1. Schematics of NanoTerasu. The 10 beamlines shown are the ones available in the first year. Blue dashed lines represent MPW beamlines, and blue solid lines represent undulator beamlines. The orange line shows the electron beam trajectory.

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110 m because it uses a compact low-emittance radiofrequency (rf) electron gun system [16] and C-band high accelerating gradient structures of more than 40 MV/m. The storage ring is also compact, with a circumference of 349 m compared with soft x-ray 3 GeV synchrotron facilities worldwide [5,7]. To achieve a horizontal emittance of 1.14 nm rad with the compact storage ring, the lattice design is a four-bend achromat with 16 cells; thus, there are 16 long straight sections and 16 short straight sections. Undulators and MPWs are installed in the long and short straight sections, respectively. Two long straight sections are used for beam injection and ring rf cavities, and two short straight sections are used for a stored beam current monitor and a bunch-by-bunch feedback system. This section briefly describes the key points of the accelerator design; the details are in the conceptual design report [15].

# A. Linear accelerator and beam transport line

Figure 2 shows a schematic of the NanoTerasu injector system, which consists of a 110-m-long 3 GeV linear accelerator section and an 80-m-long beam transport section. Stable beam injection into a low-emittance storage ring with a horizontal dynamic aperture of -15 mm requires a low-emittance injector beam from the linear accelerator.

The emittance required for the 3 GeV linear accelerator is less than 2 nm rad, corresponding to a normalized emittance of less than 10 mm mrad with a bunch charge of 0.3 nC [15]. A 50 kV dc electron gun equipped with a gridded thermionic cathode (EIMAC Y845, CPI), which has been used in many accelerator facilities, was developed to satisfy the emittance requirements and user requirements, such as equipment robustness and nearmaintenance-free operation. Although the grid degrades emittance, the transparent grid condition achieved by the optimized cathode grid voltage allows the generation of a low-emittance beam [16]. Emittance growth due to space

charge effects is suppressed by immediately increasing the electron beam energy from 50 to 500 keV with a 238 MHz accelerating rf cavity placed just downstream at the 50 kV gun exit. The measured normalized emittance of the 500 keV electron beam is 1.7 mm mrad in the core part, which contains 60% of the 1 nC bunch charge, satisfying the requirements as an electron source not only for the NanoTerasu injector but also for a soft x-ray free-electron laser. The 500 keV electron beam is bunch-compressed by a 476 MHz subharmonic buncher (SHB) from 500 to 5 ps FWHM and accelerated up to 40 MeV in a 2-m-long S-band accelerating structure.

The main acceleration section consists of 20 C-band accelerating units, which provide efficient acceleration from 40 MeV to 3 GeV. In a single unit, the 50 MW, 2.5 µs rf output from the klystron [17] is increased to 180 MW by an rf pulse compression cavity (SLED [18]) and fed into two 2-m-long C-band accelerating structures. The C-band accelerating units achieve an acceleration gradient of 42 MV/m. A MicroTCA.4 system for precise low-level rf control of the C-band units is used to obtain high electron beam stability and reproducibility. The MicroTCA.4 system enables high-density implementation and high-speed signal processing. It consists of a highspeed digitizer (250 MS/s) and an rf front-end with eightchannel input and one-channel vector modulated output. The system monitors the rf power and phase of the lowlevel amplifier output, klystron input/output, SLED output, traveling wave output to the accelerating structure, and reflected wave. The rf frontend has adjustable rf attenuation from 0 to 31.5 dB in steps of 0.5 dB, and compensation parameters for the phase difference due to this attenuator are measured in advance. The attenuator of the accelerating structure is set to 0 dB during the beam-induced signal measurement shown in Sec. III A.

The electron beam from the 3 GeV linear accelerator is transported to the storage ring through an 80-m-long beam transport section. The electron beam is transported through

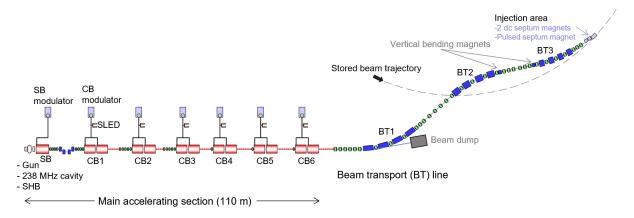


FIG. 2. Diagram of the linear accelerator and beam transport line of NanoTerasu. S-band and C-band (CB) modulators, and six CB sections with only each first unit are shown. The beam transport line consists of three sections from the exit of the linear accelerator to the injection area: BT1, BT2, and BT3. Bending (blue) and quadrupole (green) magnets are shown.

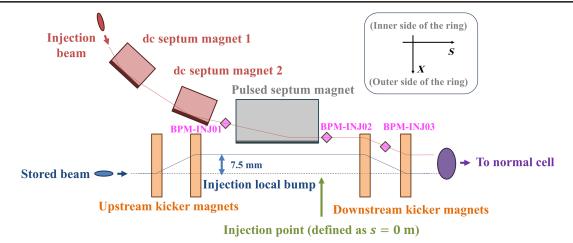


FIG. 3. Schematic of the storage ring injection area. A stored beam going from the left side of this figure is kicked by pulse kickers, and a 7.5-mm-high local bump is produced horizontally. An injection beam from the beam transport line comes from the upper side of this figure and is curved horizontally into the inner side of the ring by two dc septum magnets and a pulsed septum magnet. The injection beam can be monitored by the three beam-position monitors (BPMs).

three deflection sections horizontally and one deflection section vertically. The deflection sections are formed under an achromatic condition, in which the dispersion function of each deflection section is locally closed on the order of several tens of millimeters. The electron beam along the beam transport line traveled under the storage ring beam trajectory. Two vertical bending magnets lift up the electron beam by a height of 600 mm between the BT2 and BT3 sections. In the BT3, the injection beam asymptotically approaches the stored beam trajectory for the storage ring injection point.

## **B.** Beam injection

An in-vacuum off-axis beam injection system from the ring inside is used for stable and transparent beam injection and to allow top-up operation [19]. The injection system shown in Fig. 3 consists of two compact dc septum magnets with a recently proposed low-current-density design [20], an in-vacuum pulsed septum magnet, and a pair of twin kickers with identical magnetic characteristics thanks to a new iron lamination scheme with additional interlaminar insulation [21]. The system is designed to allow a small oscillation amplitude of the injected electron beam and a stored beam oscillation amplitude less than 10  $\mu m$ , satisfying transparent beam

TABLE I. Parameters of the storage ring injection magnets [15].

	dc septum	Pulsed septum	Kicker
Magnetic field (T)	1.2	1.4	0.2
Effective length (mm)	400	500	300
Integrated field (Tm)	0.48	0.70	0.06
Kick angle (mrad)	48.0	70.0	6.0
Pulse width (μs)	•••	10	3

injection during top-up operation. The bumped beam trajectory is 7.5 mm from the nominal position horizontally. The septum wall of thickness 0.5 mm is 2.5 mm from the bumped stored beam. The length and kick angle of each kicker are 300 mm and 6 mrad, respectively. Those of the pulsed septum are 500 mm and 70 mrad, and those of the dc septum are 400 mm and 48 mrad. The parameters are summarized in Table I.

Two dc septum magnets are powered in series by a single power supply. Twin kickers are driven by a single solid-state pulser to generate identical kicker magnetic pulses [22]. The pulser consists of a charging circuit up to 55 kV, a main capacitor of 65 nF, and a fast IGBT switch and provides a half-sine pulse-shaped current with a 1.6 kA peak and 3 µs width. The fluctuation of the charging voltage is measured as 0.01%, indicating good reproducibility. The magnetic properties of the kickers, such as inductance, should be identical [21]. The difference between the measured temporal profiles of the magnetic fields of the twin kickers is  $\pm 0.1\%$ , satisfying the specification, corresponding to  $\pm 6 \mu rad$  kick uncertainties. Ceramic vacuum chambers with uniform titanium coating of  $3 \pm 0.1 \, \mu m$  in thickness are used. The magnetic field is attenuated by 3% due to the eddy current in the coating, and the attenuation is compensated for by increasing the power supply output.

The in-vacuum pulsed septum magnet has a thin septum wall 0.5 mm thick to allow the stored and injected beams to get closer for small injected-beam oscillation amplitudes. The magnet gap is 2 mm, which is narrow enough to provide a 1.4 T pulsed magnetic field uniformly along the horizontal axis over 4 mm. The stray field integral outside of the septum is reduced to  $1 \times 10^{-5}$  Tm or less by using a permalloy magnetic shield. The vacuum pressure is measured as  $\sim 5 \times 10^{-8}$  Pa. We measured the pulsed magnetic

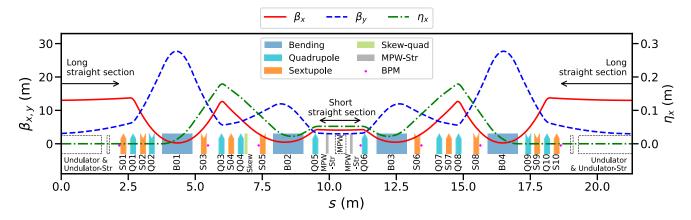


FIG. 4. Lattice functions and magnet layout for a cell. The design is symmetrical around the center, which is the MPW installation position. The horizontal axis represents the path length starting from the end of the pulsed septum magnet at the storage ring injection area.

field as a function of horizontal position with a thin search coil. The field is flat within  $\pm 0.2\%$  from 2 to 5 mm from the septum wall, where the injected beam passes. The commissioning results of the ring beam injection system are described in Sec. III B.

## C. Storage ring

The NanoTerasu lattice functions and magnet layouts for a unit cell are shown in Fig. 4, and the accelerator machine parameters are summarized in Table II. One cell consists of 4 B-Q combined bending magnets, 10 quadrupole magnets (8 focusing and 2 defocusing), 10 sextupole magnets (4 focusing and 6 defocusing), 1 quadrupole skew magnet, and 2 independent steering magnets (MPW-Str). All

TABLE II. Main parameters of the NanoTerasu storage ring four-bend achromat lattice [15].

Beam energy	2.998 GeV
Lattice	Four-bend achromat
Circumference length	348.843 m
Number of cells	16
Number of bending magnets	$4 \times 16$
Number of quadrupole magnets	$10 \times 16$
Number of sextupole magnets	$10 \times 16$
Long straight section for undulator	$5.44 \text{ m} \times 14$
Short straight section for MPW	$1.64 \text{ m} \times 14$
Betatron tune $(\nu_x, \nu_y)$	(28.17, 9.23)
Natural horizontal emittance $(\varepsilon_x)$	1.14 nm rad
Momentum compaction factor $(\alpha)$	$4.3 \times 10^{-4}$
Momentum spread $(\sigma_E/E)$	0.0843%
Bunch length (@ 0 mA)	2.92 mm
Optics at undulator center $(\beta_x, \beta_y, \eta_x)$	(13.0, 3.0, 0.0 m)
Optics at MPW center $(\beta_x, \beta_y, \eta_x)$	(4.1, 3.0, 0.05 m)
Beam current	400 mA
Energy loss in bends	0.621 MeV/turn
Accelerating radio frequency	508.759 MHz
Harmonic number	592

magnets are aligned within 50  $\mu$ m uncertainties to ensure an optics correction. Details of the magnet alignment procedures and evaluation using a laser tracker (AT403, Leica) and vibrating wire are discussed in Appendix A. The main magnet parameters are summarized in Table III.

The insertion device is placed between the cells, corresponding to the sides of Fig. 4, and the MPW is at the center of the cell. The stored beam is monitored by the button-type beam-position monitors (BPMs) [23] in which there are seven per cell.

All bending magnets (B01, B02, B03, and B04) are connected to one power supply in series, with no auxiliary power supplies or trim coils [15]. These bending magnets also have a defocusing quadrupole magnetic field (B-Q combined) in addition to the dipole field. The damping partition numbers in the horizontal, vertical, and longitudinal directions are 1.389, 1.0, and 1.611, respectively [15].

The quadrupole magnets are categorized into five families (Q01/Q10, Q02/Q09, Q03/Q08, Q04/Q07, and Q05/Q06), and each family is connected to one power supply in series. For tune correction, we use one focusing quadrupole family (Q01/Q10) and one defocusing quadrupole family (Q02/Q09) in the nondispersive sections. Five of the 10 quadrupole magnets (Q01, Q03, Q06, Q08, and Q10) have independent auxiliary power supplies for optics corrections, mainly horizontal dispersion and beta functions. The vertical dispersion and horizontal-vertical coupling can be optimized by using the skew magnets.

The sextupole magnets are also categorized into five families (S01/S10, S02/S09, S03/S08, S04/S07, and S05/S06). Each family of sextupole magnets is connected to one power supply in series. For use as steering magnets, six of 10 sextupole magnets (S01, S03, S05, S06, S08, and S10) have independent auxiliary power supplies in each pole pair. Horizontal and/or vertical magnetic fields for steering are realized by the balances of the independent three-pair (six-pole) currents. Therefore, eight horizontal/vertical steering magnets per cell, including two MPW-steering

Magnet species	Name	Effective length (m)	Strength
B-Q combined dipole	B01, B02, B03, and B04 series	1.13	0.8688 T and -7.06 T/m
	Q01/Q10 series	0.20	+32.6151 T/m
	Q02/Q09 series	0.20	-2.6278  T/m
Quadrupole	Q03/Q08 series	0.20	+49.1523 T/m
•	Q04/Q07 series	0.20	+5.4300 T/m
	Q05/Q06 series	0.20	+44.6423 T/m
	S01/S10 series	0.20	$+949.50 \text{ T/m}^2$
	S02/S09 series	0.20	$-1124.87 \text{ T/m}^2$
Sextupole	S03/S08 series	0.20	$-472.34 \text{ T/m}^2$
	S04/S07 series	0.20	$+1061.73 \text{ T/m}^2$
	S05/S06 series	0.20	$-1540.68 \text{ T/m}^2$

TABLE III. Main parameters of the NanoTerasu storage ring magnets [15].

magnets, can contribute to the closed orbit correction. The maximum kick angles for the sextupole steering magnet and MPW-steering magnet are 0.4 and 0.2 mrad, respectively. In the chromaticity correction, we use focusing (S03/S08) and defocusing (S04/S07) sextupole families in the dispersive section. The optics corrections are discussed in Secs. III F and III G.

The maximum radiation loss per turn is estimated to be 1.25 MeV, where 0.62 MeV is lost in the bending magnets, and the rest is lost in the insertion devices when an average power of 9 kW is assumed for 28 insertion devices with a nominal stored beam current of 400 mA. The maximum radiation power is evaluated to be 500 kW for a 400 mA beam. To make the Touschek lifetime longer than 5 h, an rf accelerating voltage of 3.3 MV is required. Four sets of 508.76 MHz acceleration cavities are installed on one of the 5.4-m-long straight sections. A new type of compact TM020-mode normal conducting cavity has been developed to accommodate the space limitation [24,25]. The TM020 cavity has magnetic field nodes at the TM020 acceleration mode inside the cavity. We prepared slots along the nodes and installed ferrite to damp higher-order modes (HOMs) entering the slots because the HOMs excited in the cavity cause coupled-bunch instability. HOMs are dissipated on the ferrite dampers, whereas the TM020 acceleration mode is not damped. The designed geometrical shunt impedance (R/Q) of the HOM-damped TM020-mode cavity is 113  $\Omega$  and the unloaded Q-value  $(Q_a)$  is calculated to be 60 300 [25]. The effective shunt impedance  $(R_a)$  is thus estimated to be 6.8 M $\Omega$ , and an rf power of 120 kW per cavity is required for 0.9 MV acceleration [25], which corresponds to an acceleration of 3.6 MV and an rf power of 480 kW per four cavities. Thus, a total klystron rf power of 1 MW is required to provide the maximum radiation power from a 400 mA stored beam. The beam-gap length of the cavity is 206 mm [25], and the cavity length along the beam axis can be as short as 0.5 m. The acceleration gradient of the TM020-mode cavity can be, therefore, higher than existing HOM-damped cavities [26].

#### III. BEAM COMMISSIONING

The NanoTerasu buildings were constructed from March 2019 to March 2022 in Sendai, Japan. Installation of all magnets, vacuum chambers, accelerating rf cavities, BPMs, and power supplies started in December 2021 and finished in January 2023 for the linear accelerator and in May 2023 for the storage ring. Conditioning of the accelerating cavities of the linear accelerator started on 13 February 2023 while the installation work proceeded in the storage ring tunnel. After 2 months, on April 17, 2023, we started extracting electron beams from the gun in the linear accelerator. Section III A describes the linear accelerator commissioning works up to obtaining a 3 GeV energy beam as the injector. The first electron accumulation was achieved on June 8, 2023, as described in Sec. III B. By commissioning the accelerating rf cavity (Sec. III C), vacuum (Sec. III D), and monitor (Sec. III E), we performed the optics corrections (Secs. IIIF and IIIG). Modelconsistent ring optics and a 200 mA stored beam current were obtained on October 4, 2023 by our half-year machine commissioning since the first electron beam generation by the gun. The first x-ray beam from the insertion device was obtained on December 7, 2023, and the beamline commissioning was also started in parallel. Finally, user operation began on April 9, 2024 with a stable 160 mA stored current, as described in Sec. IV. A chronological timeline with the commissioning highlights is shown in Fig. 5. In this section, we describe each accelerator machine commissioning result.

## A. Linear accelerator and beam transport line

The rf conditioning at the linear accelerator started in February 2023, and the first electron beam was generated by the electron gun in April 2023. After 10 days, we achieved a beam energy of 3 GeV with 0.3 nC and transportation to a beam dump. In May 2023, beam route was switched to the BT line going to the storage ring. In June 2023, the beam reached the end of the beam transport

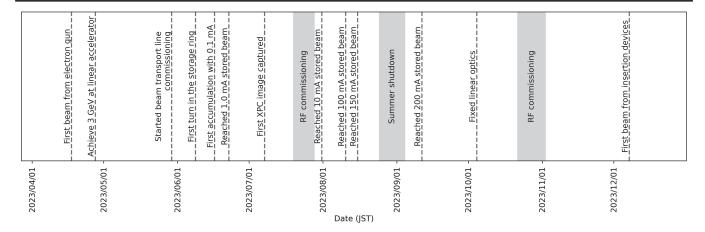


FIG. 5. Timeline from April 2023 to December 2023. Some important events are shown by vertical dashed lines. The gray shaded periods correspond to machine shutdown times.

section, where a beam profile was measured on a screen monitor between the two dc septum magnets in the storage ring injection area.

The electron beam generated in the gridded thermionic cathode is accelerated by an electric field between the anode and cathode for an energy of 50 keV. The 50 keV beam is immediately accelerated to 500 keV in the 238 MHz cavity at a crest acceleration phase. The accelerating phase and voltage of the 238 MHz cavity were optimized via a time-of-flight (TOF) measurement using two current transformers near the SHB cavity, the signals of which were measured by an oscilloscope. According to simulation results using PARMELA [27], the experimental dependence of the TOF signal on the SHB phase and voltage was adjusted. After the SHB, the electron beam is accelerated to 40 MeV in the 2 m S-band accelerating structure. The electron beam is transported through a chicane to the main C-band section. The beam-induced field is measured by the rf pickup of each C-band accelerating unit to adjust the accelerating phase and beam

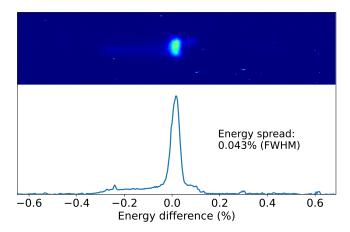


FIG. 6. Energy profile of the 3 GeV electron beam. A screen monitor and bending magnet are used for the measurement at the exit of the linear accelerator.

position. Finally, the accelerated 3 GeV beam at the exit of the C-band section is transported to the storage ring via the beam transport line.

The emittance of the accelerated 3 GeV electron beam is obtained by the quadrupole scan method [28] and is approximately 2 nm rad in both the horizontal and vertical directions. The stabilities of the bunch charge and energy for the 3 GeV electron beam are measured as 0.52% and 0.057%, respectively, which are stabilized by an rf feedback system. Figure 6 shows the energy profile of the 3 GeV beam measured using a screen monitor at the first dispersive position after the C-band section, which shows an energy spread of 0.043% (FWHM). Calibration was performed by using the dependence of the beam position on the bending magnet currents located upstream of the screen. Table IV summarizes the beam performance during beam commissioning. All beam parameters satisfy the designed values (required performance) [15] for storage ring injection.

#### B. Storage ring injection and first accumulation

Commissioning of the storage ring beam injection system was performed by using three BPMs (Fig. 3). The injection beam trajectory from the beam transport line

TABLE IV. Designed values and measurement results for the beam parameters of the 3 GeV linear accelerator. The stabilities of beam energy and charge are results using 480-shots' data.

Items	Design	Measurement
Beam energy	3 GeV	3 GeV
Bunch charge	>0.3 nC	0.39 nC
Bunch charge stability		0.52% (rms)
Horizontal emittance	2 nm rad	$1.04 \pm 0.03$ nm rad
Vertical emittance	2 nm rad	$1.84\pm0.19\mathrm{nm}\mathrm{rad}$
Energy spread	0.16% (FWHM)	0.043% (FWHM)
Energy stability	<0.2% (rms)	0.057% (rms)

was adjusted in the designed position by changing the dc septum magnet powers and monitoring with BPM-INJ01. Because the pulsed septum magnet provides a half-sine curve shape output [22], the kicked beam position also follows the half-sine curve at BPM-INJ02 if the output timing of the power supply is changed relative to the beam timing. We measured the half-sine curve beam responses and searched for the flat top timing of the shape. This method can also be adapted with BPM-INJ03 to the kicker magnets, which use the same type of solid-state power supplies. Figure 7 shows the horizontal beam-position monitored at BPM-INJ03 that was varied by changing the output timing of the downstream kicker power supply. The kicker power supply outputs a half-sine curve with a width of about 3 µs, and the expected local-bump height at the BPM-INJ03 position is about 3.5 mm. The data were consistent with the predictions, and then we optimized the pulse output timings.

The parallelism of the injection beam with respect to the designed stored beam trajectory was tuned using BPM-INJ02 and BPM-INJ03. Turning off the downstream kickers and turning on only the pulsed septum should give the same horizontal beam position between BPM-INJ02 and BPM-INJ03. We adjusted the pulsed septum power as described above.

After optimizing the injection timings and powers, we led the beam into the storage ring. Owing to the excellent magnet alignment described in Appendix A, the electron beam traveled over 300 turns in the storage ring with no steering magnet kicks on June 8, 2023.

Figure 8 shows a turn-by-turn horizontal beam position at one of the dispersive sections ( $\eta_x = 0.09$  m) and BPM intensity with no rf power. After around 300 turns, the electrons spread concentrically, and the observed beam position appeared near the center. At around 330 turns, the BPM signal intensity reached the background level because the beam was lost. The measured beam positions and betatron oscillation almost agreed with the simulation,

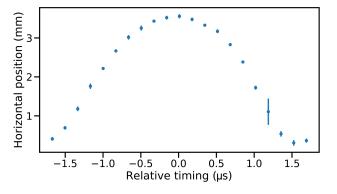


FIG. 7. Injection beam positions as a function of the kicker pulse output timing. The horizontal axis represents the relative timing from the center of the figure set to 0  $\mu$ s. The error bar also includes the stability of the injection beam position from the linear accelerator.

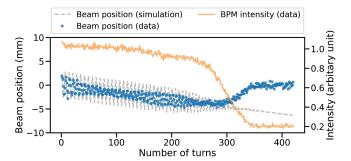


FIG. 8. Turn-by-turn horizontal beam position (blue) and BPM intensity (orange) at a dispersive section BPM without rf power. The gray dashed line corresponds to simulated beam positions with ideal injection beam optics. In the simulation, 1000 electrons are tracked with the model storage ring parameters.

except for the amplitude damping, although the accelerator machines were under commissioning. It is suspected that these deviations were caused by the incident beam energy and optics. The beam transport and linear accelerator sections can still be adjusted to address these discrepancies.

We achieved the first capture and storage of an electron beam on June 16, 2023 after turning on the rf power and optimizing its phase. The first accumulated beam orbit is discussed in Sec. III F. This is the first ring beam acceleration by a TM020-mode cavity to our knowledge, and details of the conditioning of TM020-mode cavities are described in Sec. III C.

Owing to the well-established beam transportation in the beam transport line and linear accelerator commissioning, the injection beam charge into the storage ring is  $\sim$ 0.3 mA per shot, corresponding to an injection efficiency of  $\sim$ 88%. One of the usual beam storing processes up to 160 mA is shown in Fig. 9. Figure 10 shows the injection beam profiles monitored by a BPM at one of the dispersive sections to estimate the synchrotron phase. The beam position oscillates  $\sim$ 2 mm at the injection timing but converges to less than 0.5 mm after  $\sim$ 30 turns. In contrast, at the BPM near the undulator positions where there is the dispersion-free section, the converged horizontal oscillation is less than  $\pm$ 0.1 mm after  $\sim$ 30 turns. The beam is injected at the center of the separatrix.

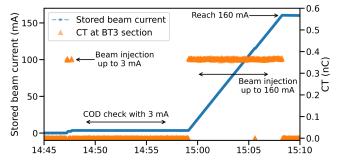
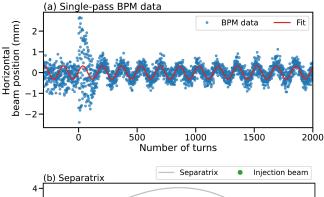


FIG. 9. Stored beam current (blue dots) and injection charge per shot in 1 Hz monitored at the BT3 section (orange triangles).



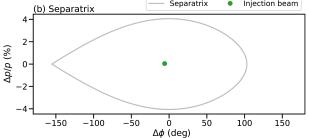


FIG. 10. (a) Injection beam-position data observed by a single-pass BPM at the dispersive section in the storage ring. The red line represents a fitting result with a cosine function to estimate the beam phase. (b) Injection beam synchrotron phase  $(\Delta\phi)$  and energy differences  $(\Delta p/p)$ . The separatrix is drawn assuming an accelerating voltage of 2.9 MV (Sec. III C). The injection beam has little energy discrepancy as  $\Delta p/p = 0.046\%$  and synchrotron phase as  $\Delta\phi = -5.9$ °.

## C. Storage ring rf commissioning

Four HOM-damped TM020-mode cavities were manufactured and delivered to SPring-8 each in order from June to December 2020 [29]. Because the NanoTerasu site was still under construction in 2020, the first cavity studies were started at the SPring-8 site. The number and position of HOM dampers embedded in each cavity were determined by measuring cavity *Q*-value with a low-power test at SPring-8. The HOM damper consists of 12 HF70 ferrite bars brazed onto a copper block cooled with cooling water [25,29]. The copper block is brazed onto a stainless steel flange. The HF70 is a Ni-Zn-based ferrite produced by

TDK Co. with a high imaginary part of permeability suitable to absorb rf fields in the 0.2-3 GHz frequency range [30]. The size of the ferrite bar is  $25.5 \text{ mm} \times$ 10.26 mm × 4 mm. Some of the HOM dampers close to coupler ports, tuners, and the opposite side of tuners were found to decrease Q-values due to the absorption of a small portion of rf fields at the fundamental TM020-mode. The HOM damper absorbing more than about 0.3% to 0.5% of the rf power at the fundamental TM020-mode was removed from the cavity to avoid too much self-heating because the ferrite's permeability sharply drops to zero when exceeding its Curie temperature, > 100°C for HF70 ferrite. The ferrite bar loses its performance as rf absorbers above Curie temperature. The number and position of HOM dampers installed in the cavity are different from each cavity, as shown in Fig. 11 and as listed in Table V together with cavity Q-values with and without HOM dampers. The difference is considered to come from the manufacturing accuracy of the cavity, and the detailed reason is under investigation. Dummy flanges made of stainless steel were installed as a vacuum seal where HOM dampers were removed. Those dummy flanges will not absorb rf fields at any mode.

The cavity made of oxygen-free high-conductivity (OFHC) copper is equipped with a cooling water system to mitigate thermal expansion of the cavity caused by input rf power of up to more than 100 kW. A frequency tuner made of OFHC copper block with a diameter of 70 mm and stroke of -10 to 40 mm is mounted on the side of the cavity to keep the frequency to 508.76 MHz by compensating the frequency shift caused by thermal expansion of the cavity and beam loading with the tuning range of about 0.3 MHz [25]. An rf coupler port with a variable coupling mechanism located at the top of the cavity is connected with an rf waveguide, which is vacuum sealed by an rf window made of low-loss ceramic (Kyocera A479B) [25,29]. The assembled cavity was evacuated by a turbopump and baked at 120 °C for 20 h. A nonevaporable-getter pump (NEG) and ion combination pump, NEXTorr D500, were activated at the end of baking. High-power conditioning was then performed up to 100 kW per cavity with the

TABLE V. The positions of HOM dampers initially installed at each cavity. The numbers and positions correspond to the ones shown in Fig. 11.

Cavity number	Installed position number	Q-value without HOM dampers	Q-value with HOM dampers
Cavity 1	2, 3, 4, 5, 6, 7, and 8 (upstream side) 2, 3, 4, 5, 6, 7, and 8 (downstream side)	58 700	58 900
Cavity 2	2, 4, 5, 6, and 8 (upstream side) 2, 4, 5, 6, and 8 (downstream side)	59 300	59 300
Cavity 3	2, 4, 5, and 8 (upstream side) 2, 5, and 8 (downstream side)	59 900	59 900
Cavity 4	<ul><li>2, 5, and 8 (upstream side)</li><li>2, 5, and 8 (downstream side)</li></ul>	59 700	59 900

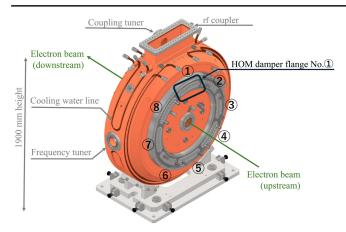


FIG. 11. Storage ring rf cavity design and numbering of the HOM damper flanges view from the beam upstream side. The numbers 1–8 align counter-clockwise. The same number of HOM damper flanges is aligned on the downstream side and clockwise view from the downstream side.

configuration of HOM dampers listed in Table V. It took about 40 days per cavity from the start of conditioning to the steady-state operation at 100 kW without any failure for more than a week [29].

All four high-power conditioned cavities up to 100 kW were transported to the NanoTerasu site from SPring-8 in March 2023 and installed in the designed positions along a 5.4-m-long straight section as shown in Fig. 12, which has gate valves at both ends to separate the straight section from the other part of the storage ring. The distance between adjacent cavity centers is chosen to be 0.884 m corresponding to one and a half wavelength of the fundamental frequency of the cavity at NanoTerasu, taking into account of installation of the cavities and implementation of necessary components. Two synchrotron radiation absorbers and five NEXTorr D500 are installed along the beam pipe of the four cavities. The 1.13 m space downstream of the four cavities is kept in reserve to install a longitudinal feedback system for suppression of coupled-bunch instability or a higher harmonic cavity to lengthen the bunch length. Cavity numbers 1–4 are along with the electron beam from upstream to downstream. After all the vacuum chambers between the gate valves and all the vacuum components,

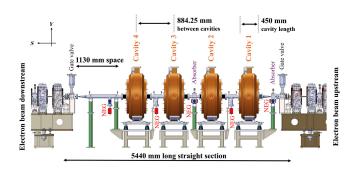


FIG. 12. Schematic of the storage ring rf cavity section.

such as ceramic rf windows, couplers, tuners, pickups, vacuum pumps, and vacuum gauges, were assembled with the cavities, the cavity system along the long straight was evacuated by turbopumps and baked at  $120\,^{\circ}\text{C}$  for 20 h again. NEG pumps were activated at the end of baking, and ion pumps were switched on. The vacuum pressure in the cavities reached less than  $4 \times 10^{-7}$  Pa in the middle of May 2023, 1 month after the baking.

A continuous wave klystron at 509 MHz with a maximum average power of 1.2 MW, E3732 manufactured by Canon Electron Tubes & Devices Co., Ltd., is used as an rf source to feed the rf powers into four cavities. The source rf power is equally split and provided into the four cavities with an rf transmission system composed of waveguides and magic tees [15]. The amplitude and phase of the total acceleration voltage determined by the vector sum of four cavities are stabilized by a low-level rf control system, which is similar to that developed at SPring-8 to control an rf system composed of eight cavities and a single klystron [15,31].

The rf conditioning of four cavities started at the end of May 2023. As the rf conditioning progressed, we gradually increased the input rf powers. By the time we achieved the first electron beam accumulation on June 16, 2023, the total power of the four cavities had reached 200 kW, and by mid-July, it had reached a maximum of 400 kW without an electron beam, as shown in Fig. 13. The accelerating voltage and rf power are set to be 2.9 MV and 320 kW, respectively, for the initial phase of user operation with 10 insertion device beamlines. The accelerating voltage of 2.9 MV is realized for nominal daily operation with an effective length of 3.54 m, which is a fourfold distance between adjacent cavities, as shown in Fig. 12. The high accelerating voltage achieved with compact length would be epoch-making as a HOM-damped normal conducting cavity system. The bunch length spreads to 3.3 mm from a designed value of 2.9 mm for the accelerating voltage. The rf momentum acceptance is estimated to be 3.7% when 10 insertion devices are operated with an average power of 9 kW (Fig. 14). This acceptance is similar to 3.5%

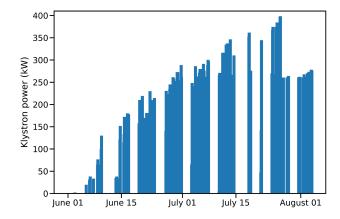


FIG. 13. Progress of the total power of four rf cavities in 2023.

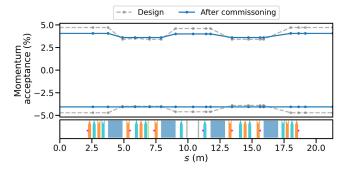


FIG. 14. Momentum acceptance estimation in a cell. The gray line shows the momentum acceptance with a designed accelerating voltage of 3.6 MV and designed chromaticities of  $(\xi_x, \xi_y) = (1.38, 1.53)$ . The blue lines show ones with after-commissioning parameters of 2.9 MV accelerating voltage and  $(\xi_x, \xi_y) = (1.98, 1.98)$  configurations. The bottom panel displays magnet and BPM positions as shown in Fig. 4.

evaluated for the 3.2 MV accelerating voltage with full operation of 28 insertion devices discussed in Sec. II C, where a Touschek lifetime longer than 5 h is anticipated.

# D. Storage ring vacuum

Optics corrections and beam monitor commissions began in the daytime with a stored beam current of 10 mA or less. For vacuum conditioning, we started night operation in August 2023 with a stored beam current of over 10 mA. We gradually increased the stored current for the vacuum conditioning, as the maximum stored current was updated in daytime commissioning (Fig. 5). Finally, we performed 200 mA stable operation over the whole night. Figure 15 shows the progress of the vacuum conditioning in the storage ring. We obtained a beam lifetime of over 5 h with a stored beam configuration of 200 mA until December 2023. Moreover, by continuing the vacuum conditioning while commissioning the

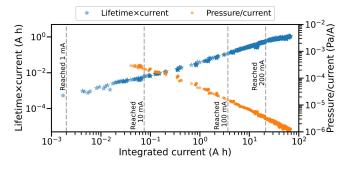


FIG. 15. Electron lifetime and ring vacuum pressure for a half year. Lifetime multiplied by the stored beam current grows with respect to an integrated current. Pressure normalized by the stored beam current decreases with respect to the integrated current. The pressure value is taken from a cold-cathode gauge near the photon beam absorber. The gray vertical dashed lines correspond to some milestones of the maximum stored beam current.

accelerator and beamlines, the electron beam lifetime reached  $\sim 10$  h, which is a sufficiently long time for the first year of user operation.

# E. Storage ring BPM

Beam positions are monitored by seven BPMs per cell (Fig. 4). These BPMs are mounted on the vacuum chambers; therefore, there is a little range in their independent alignments. The vacuum chambers were aligned by the laser-tracker measurement, with priority on the alignment of the photon beam absorber positions. The laser-tracker accuracy is better than 50 µm in our configuration, but the manufacturing uncertainty between the mechanical and electrical centers of BPMs is about 100 µm. To ensure the precise beam position, the beam-based alignment (BBA) method [32] is essential. Figure 16 shows the BPM offsets obtained by BBA using quadrupole magnets. The most distant horizontal and vertical offsets are -578 and -450 μm, respectively. The mean value and standard deviation of laser-tracker measurements for horizontal (vertical) are -13.89 (1.38) and 101.46 (93.10  $\mu$ m), respectively. Those of the BBA are -66.82 (-36.07) and 146.61 (138.42 μm), respectively.

Hereafter, beam positions are corrected by using the above results.

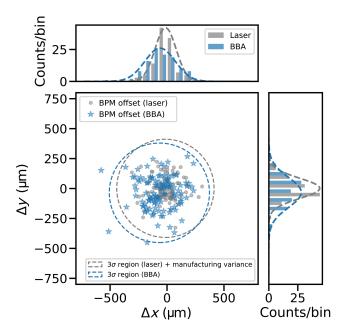


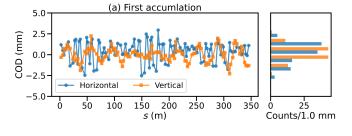
FIG. 16. BPM offsets from the BBA and laser-tracker measurements. The top and right panels represent the one-dimensional projected histograms horizontally and vertically. Dashed curves in the top and right panels are Gaussian fitting results. The blue dashed ellipse in the left bottom panel is a  $3-\sigma$  region from the Gaussian fitting results. The gray dashed ellipse is a  $3-\sigma$  region from the Gaussian fitting results, considering the manufacturing uncertainty among the BPM electrodes and laser-tracker basepoint.

## F. Closed orbit and tune correction

To correct the ring optics to the designed model, we performed the following steps: closed orbit distortion (COD) correction, circumference length correction, betatron tune correction, rough horizontal dispersion correction, chromaticity correction, and dispersion and beta function correction using a linear optics correction. This section describes the optics corrections except for the beta function correction. In the next section, we discuss the ring optics and error sources with dispersion and beta function correction.

Figure 17(a) shows the (COD) at the first electron beam accumulation on June 16, 2023. The first COD was a vertical spread of  $\sim \pm 2$  mm compared with the vacuum chamber height of  $\pm 8$  mm for the normal cell and  $\pm 4.5$  mm for the insertion device sections. The chamber width is  $\pm 15$  mm, which was wide enough for the first horizontal spread of  $\pm 3$  mm. Details of the vacuum chamber are described in the conceptual design report [15].

Figure 18 shows the dipole kick powers horizontally and vertically for the COD corrections. The biggest kick



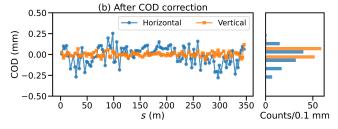


FIG. 17. Closed orbit at the first electron beam accumulation in the storage ring (a), and after COD and other optics corrections (b), monitored by the 112 BPMs in the storage ring. (a) The horizontal (vertical) mean values and standard deviations are 0.44 (-0.01), and 1.17 (0.84 mm), respectively. (b) The horizontal (vertical) mean values and standard deviations are -0.01 (0.00) and 0.11 (0.03 mm), respectively.

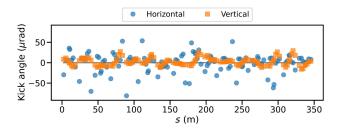


FIG. 18. Horizontal and vertical kick angles applied by all steering magnets.

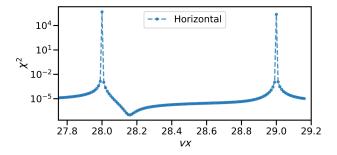
was  $\sim \!\! 80 \, \mu rad$ , which is sufficiently small for the power supplies, which have a maximum designed power of 400  $\mu rad$  [15]. Figure 17(b) shows the COD after the corrections. The deviations became 1/10 both horizontally and vertically, and the mean values were centered.

The betatron tune is particularly important. We can monitor the fractional betatron tune using the bunch-by-bunch feedback. However, in case that the tune is a half-integer different from the designed value, the steering magnet responses work in the opposite direction. To confirm the tune, we use the beam responses. A steering magnet applied a small kick to the beam, and we estimated the tune by fitting the COD differences with the model. Figure 19 shows the fitting results. The evaluation function is defined as

$$\chi^2 \equiv \sum_{m} [\Delta x_m^{\text{COD}} - \Delta x_m^{\text{Model}}(\nu)]^2, \tag{1}$$

where  $\Delta x_m^{\rm Model}(\nu)$  is the COD differences as a function of the betatron tune with a steering kick of the *m*th magnet calculated from the model. The estimated horizontal tune  $(\nu_x)$  and vertical tune  $(\nu_y)$  are 28.16 and 9.25, respectively. These tunes were corrected to 28.17 and 9.23 as the designed values by changes in one of the focusing series (Q1/Q10 series) and defocusing series (Q02/Q09 series) of the quadrupole magnets.

The dispersion function  $(\eta)$  was measured by changing the rf to  $\pm 300$  Hz. The horizontal dispersion is corrected by tuning the quadrupole magnets, which are aligned at the dispersive section. Those correction quadrupole magnets are also involved in the beta function correction, but we modified only the horizontal dispersion function in



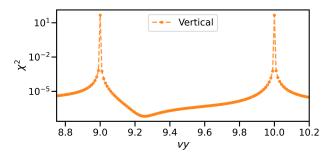


FIG. 19. Tune estimation using kicked COD changes for horizontal (upper panel) and vertical (lower panel) tune.

the first step. The original horizontal dispersion was partially large in one of the long straight sections, which are dispersion-free sections in the design. The radiation monitor detected beam loss at that section, but the first dispersion correction resolved it.

The vertical dispersion is produced by quadrupolemagnet rotation errors. This was corrected by the skew quadrupole magnets.

The horizontal and vertical chromaticities  $(\xi_x, \xi_y)$  are measured by the tune shift with rf changes. The original vertical chromaticity was close to 0, and the stored beam was unstable at the higher current. The chromaticity correction was performed with the focusing (S03/S08 series) and defocusing (S04/S07 series) sextupole magnet. For stable operation in the commissioning phase and the first user operation, the modified chromaticities are adjusted to slightly higher values from the designs,  $(\xi_x, \xi_y) = (1.98, 1.98)$ . Although the present configuration has higher chromaticity than the conceptual design, the beam injection efficiency was not different from that of a configuration fitting the designed value.

# G. Linear optics correction

In Sec. III F, we performed the optics corrections in individual steps independently. These processes are essential to close the storage ring responses in the designed model. However, the changes in the quadrupole magnets for tune corrections and dispersion corrections affect the changes in the beta functions. This section discusses the simultaneous correction for the dispersion and beta function.

Using a fundamental idea of linear optics correction [33], we measured all response functions with each steering magnet applying a 30 µrad kick and estimated the ring optics with errors for the storage ring. Comparing the computed and measured responses, we estimate plausible error sources and obtain the optics parameters under those conditions. We used EIGEN version 3.4 [34] for solving the matrices by singular value decomposition.

For easy confirmation of the ring responses in the firstyear operation, we only modified the quadrupole magnet fields. The correction coefficients obtained for the auxiliary power supplies are shown in Fig. 20.

Figure 21 compares the beta functions before and after the correction and the model. Although the beta functions were a maximum of  $\sim$ 2.0 m different from the model before the quadrupole power error corrections, they became consistent within  $\sim$ 0.2 m from the design after the modifications. The horizontal dispersion functions were also modified (Fig. 22). The discrepancy of the horizontal dispersion was  $\pm$ 0.05 m before the correction, but it became consistent within  $\pm$ 0.009 m. The vertical dispersion was then independently corrected by using skew magnets, as described in Sec. III F. The vertical dispersion

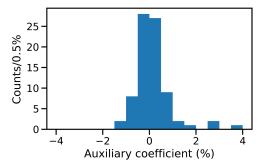


FIG. 20. Relative quadrupole magnet fields from the designed values, which the auxiliary power supplies used for the optics correction. Although one magnet was adjusted by a maximum of +4%, the mean of the correction factor is 0.15%.

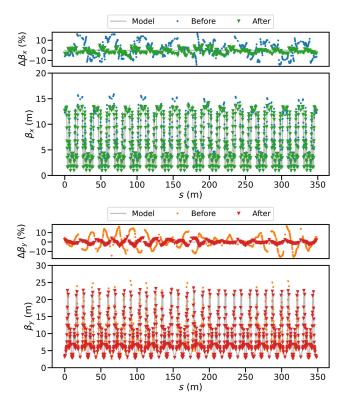


FIG. 21. Horizontal (upper panels) and vertical (lower panels) beta functions before and after correction. The top panel of each figure shows the discrepancy from the designed model.

function had a difference of  $\pm 0.03$  m and was modified within  $\pm 0.003$  m.

As a result, the discrepancies of the horizontal and vertical dispersions and beta functions reached 1/10, and our storage ring satisfied the optics parameters sufficiently to start the first-year operation as a synchrotron facility. We applied the modification only to the quadrupole magnet and not to the BPMs and steering magnets for their rolling and gains, and thus the remaining discrepancies probably originated from these sources. Their gain (roll) errors are estimated to be a maximum of approximately

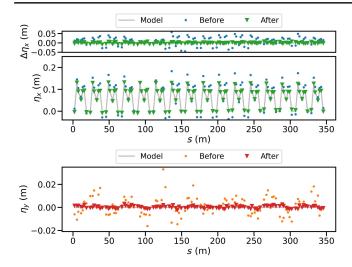


FIG. 22. Horizontal (upper panels) and vertical (lower panel) dispersion functions before and after correction. The top panel in the horizontal dispersion shows the difference from the model. Because the vertical dispersion is 0 m in the design, the bottom panel corresponds to the difference.

 $\pm 10\%$  ( $\pm 4\%$ ). We plan to continue optimizing the storage ring step-by-step during machine maintenance time soon.

## H. Beam size

We have a three-pole wiggler installed in one of the short straight sections to monitor the beam size. The wiggler radiation is observed by an x-ray pinhole camera (XPC). This beam-size monitoring system was developed for the SPring-8-II project [10], and details are given in Ref. [35]. The spatial resolution of the monitoring systems is  $\sim$ 4  $\mu$ m for 50 keV x-ray conditions [36]. In our commissioning configuration with different x-ray energy spectra from the study, the net resolution of the monitoring system is  $\sim$ 6  $\mu$ m.

Figure 23 shows the beam profile monitored by the three-pole wiggler and XPC. By projecting into one dimension and fitting with the Gaussian function, we found that the horizontal and the vertical beam sizes are 83.9 and 9.1  $\mu$ m, respectively. The emittance ( $\epsilon$ ) and energy spread ( $\sigma_E/E$ ) are calculated by

$$\sigma_{\text{beam}} = \sqrt{\left(\eta \cdot \frac{\sigma_E}{E}\right)^2 + \beta \cdot \varepsilon},$$
 (2)

where  $\sigma_{\rm beam}$  is the  $1-\sigma$  beam size, and  $(\eta, \beta)$  are the optics parameters at the three-pole wiggler position. We obtained the energy spread as  $(\sigma_E/E) = (0.0972 \pm 0.0161)\%$  assuming a model emittance of 1.14 nm rad, that is,  $1\sigma$  consistent within the designed value of 0.084%. The included uncertainties are the discrepancies of the beta function and dispersion between the designed model and the measurement after the correction (Figs. 21 and 22).

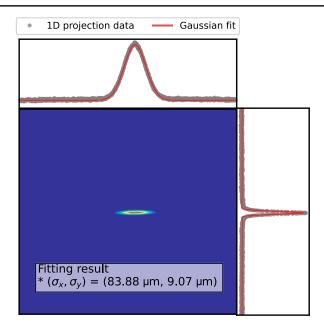


FIG. 23. Stored electron beam profile obtained from the XPC with a stored beam current of 10 mA. Horizontal and vertical beam sizes are estimated from the Gaussian fitting for the one-dimensional projection distributions. These figure axes show the XPC pixels, but the fitting results include the conversion into the actual size of 0.96  $\mu$ m/pixel. The horizontal and vertical axes are arbitrary in this figure and do not directly reflect the beam position in the storage ring.

In contrast, assuming the designed value of the energy spread, the horizontal and vertical emittances are 1.29 and 0.03 nm rad at the three-pole wiggler position, respectively. The coupling between the horizontal and vertical emittances is estimated to be  $\sim$ 2.1%. Because the emittance and energy spread are convoluted, they cannot be determined as unique values from the XPC results alone. A future challenge is to use the insertion devices to confirm the compensation between them [37].

On the other hand, the horizontal beam size at XPC became larger than double at high current due to a beam instability. We speculated that a coupled-bunch instability occurred in HOM-damped TM020-mode cavities, resulting in a large energy spread, because HOM dampers were not fully installed inside cavities as listed in Table V. We, therefore, added HOM dampers to cavities 2, 3, and 4 in November 2023. The number of HOM dampers is 14 for each cavity, and the positions are the same as cavity 1. The HOM dampers near the coupler port remain removed because the decrease in the Q-value was significant. However, the instability-threshold current did not improve so much upon the additional HOM dampers. Further investigation is underway to increase the instabilitythreshold current. Figure 24 shows stored beam current and beam size for a whole night in November 2023 with 14 HOM dampers per cavity. When the stored current reached about 230 mA, the horizontal beam size doubled.

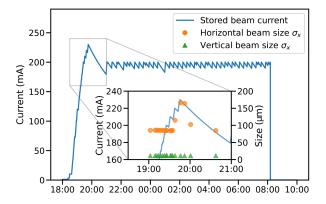


FIG. 24. Stored beam current and beam size observed by XPC. The stored beam reached 230 mA at maximum and kept 190–200 mA operation for the whole night. The horizontal and vertical beam sizes are estimated from the XPC data using Gaussian fitting.

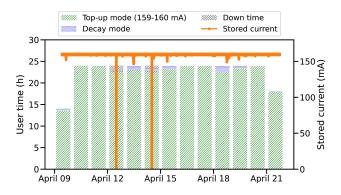


FIG. 25. User time and downtime in the first user operation period from April 9, 2024 10:00 to April 21, 2024 18:00 (JST).

We conservatively decided to provide 160 mA configuration for the first user operation from April 2024.

#### IV. FIRST USER OPERATION

On April 9, 2024 10:00 (JST), the first user time began at NanoTerasu. The stored current was kept at 159–160 mA by top-up operation, and the undulators kept their gaps working while the beam was injected. The beam lifetime is approximately 10 h, and the beam injection is performed a few times with a 1 Hz injection every several minutes. During user operations, we automatically perform the COD correction, circumference length correction, and tune correction (Sec. III F). Counter kicks for undulator workings are corrected by feed-forward correction, in which the discrepancies from the normal orbit are less than  $\sim\!\!\pm10~\mu m$ .

Figure 25 shows the history of the stored current in the user operation period and user service times. Recent operation status can be viewed on the NanoTerasu web page [11]. Until the end of the first user time on April 21, 2024 at 18:00, we experienced beam losses twice due to problems with the storage ring rf cavity reflection. Because rebooting the rf power to the operational value takes about 1 h, the total downtime was about 2 h, corresponding to 0.6% of the total user time in the first period. rf power reflections in the linear accelerator also occurred, and the top-up operation was suspended for several minutes several times. Thus, we achieved 99.4% user service time in the first period and maintained top-up operation (stored current is more than 159 mA) in 98.0%

TABLE VI. Brief summary of the storage ring commissioning. The beam energy and emittances are assumed to be the designed values. x and y represent the horizontal and vertical, respectively.

Parameter	Design	After commissioning
Energy	2.998 GeV	2.998 GeV <sup>a</sup>
Circumference length $(C)$	348.843 m	348.843 m
Beam current	400 mA	≧200 mA
Betatron tune $(\nu_x, \nu_y)$	(28.17, 9.23)	$(28.17 \pm 0.01, 9.23 \pm 0.01)^{b}$
Chromaticity $(\xi_x, \xi_y)$	(1.38, 1.53)	(1.98, 1.98)
Beta function $(\beta_x, \beta_y)$ at the long straight section	(13.0, 3.0 m)	$(13.0 \pm 0.3 \text{ m}, 3.0 \pm 0.05 \text{ m})$
Dispersion $(\eta_x, \eta_y)$ at the long straight section	(0.0, 0.0  m)	$(0.0 \pm 0.004 \text{ m}, 0.0 \pm 0.001 \text{ m})$
Beta function $(\beta_x, \beta_y)$ at the short straight section	(4.1, 3.0 m)	$(4.1 \pm 0.1 \text{ m}, 3.0 \pm 0.05 \text{ m})$
Dispersion $(\eta_x, \eta_y)$ at the short straight section	(0.05, 0.00  m)	$(0.05 \pm 0.004 \text{ m}, 0.00 \pm 0.001 \text{ m})$
$COD(\Delta x, \Delta y)$		$(-0.01 \pm 0.11 \text{ mm}, 0.00 \pm 0.03 \text{ mm})^{b}$
Coupling	1%	2.1%
Emittance $(\epsilon_x, \epsilon_y)$	(1.14, 0.01 nm rad)	$(1.14 \text{ nm rad}^{a,c} 0.02 \text{ nm rad}^{d})$
Energy spread $(\sigma_E/E)$	0.0843%	$0.0972 \pm 0.0161\%$
Bunch length $(\sigma_b)$	2.92 mm (9.74 ps)	3.3 mm (10.9 ps)
Filling pattern	•••	1–400 buckets
Electron lifetime	•••	~10 h @ 160 mA

<sup>&</sup>lt;sup>a</sup>Assuming the designed value.

<sup>&</sup>lt;sup>b</sup>Converged by a consistent correction in operation.

c1.29 nm rad assuming the designed energy spread of 0.0843%.

<sup>&</sup>lt;sup>d</sup>Estimated from the obtained coupling constant and the model horizontal emittance.

of the time; the assigned user service time was 296 h, and the total downtime was 1.87 h.

### V. SUMMARY AND FUTURE PROSPECTS

As shown in the timeline (Fig. 5), we achieved a stored beam current of 200 mA on September 11, 2023. In that configuration, we can provide a model-consistent storage ring for user operation. For user operation from April 2024, we started with a stored beam current of 160 mA, which is 80% of our stable configuration of 200 mA. The beam instability and the beam size spread over 200 mA were found. We tried to improve the instability-current threshold by additionally installing the HOM dampers for the storage ring rf cavities, but this did not change the situation. The solutions for this to achieve 400 mA of stored current are under investigation.

The storage-ring rf accelerating voltage of 2.9 MV is lower than the designed value of 3.6 MV but is adequate for the present number of beamlines. To build new beamlines in the future, we must increase the rf power and perform conditioning on that power.

The coupling constant was not tuned during the present commissioning period but converged with approximately double the designed value. This will be improved by using skew magnets and the closest difference resonance of  $\nu_x - \nu_y = 19$ , although we must consider the balance between the Touschek beam lifetime and the vertical emittance, which will be required by beamline users in the future.

The chromaticities are set to be slightly larger than the designed values and will be modified to the designed values while monitoring the beam stability at a higher stored current.

The key point of the short-timeframe commissioning in the storage ring optics was the fine-aligned magnets in the storage ring. These magnets allowed us to omit the firstturn steering and easily converge the ring optics into the linear beam responses.

The machine commissioning results for the half a year are summarized in Table VI. We achieved model-consistent ring optics, and those parameters will help design a future undulator beamline in NanoTerasu using the SPECTRA simulation tool [38].

## **ACKNOWLEDGMENTS**

We thank all members of the Photon Science Innovation Center (PhoSIC) and QST NanoTerasu Center for their help and fruitful discussions over the whole commissioning period. We also greatly appreciate that many companies have been dedicated to accelerator complex constructions for several years. We express our sincere thanks to Drs. K. Soutome (JASRI, RIKEN) and T. Fukui (RIKEN) for their helpful discussions. We thank ThinkSCIENCE, Inc. (Tokyo, Japan) for English language editing.

# APPENDIX A: MAGNET ALIGNMENT IN THE STORAGE RING

The magnet alignment is vital to the linear optics correction in the storage ring. An alignment error causes additional dipole kicks in quadrupole magnets and quadrupole kicks in sextupole magnets. Their contributions to COD and the beta function are

$$\Delta x^{\text{mon}} = \frac{\sqrt{\beta_x^{\text{mon}}}}{2\sin(\pi\nu)}\cos(\pi\nu - \Delta\psi_x)\sqrt{\beta_x^{\text{mag}}}kL\Delta x^{\text{mag}}, \quad (A1)$$

$$\Delta y^{\rm mon} = \frac{\sqrt{\beta_y^{\rm mon}}}{2\sin{(\pi\nu)}}\cos{(\pi\nu - \Delta\psi_y)}\sqrt{\beta_y^{\rm mag}}kL\Delta y^{\rm mag}, \quad (A2)$$

$$\Delta \beta_x^{\text{mon}} = \frac{\beta_x^{\text{mon}}}{2\sin(\pi \nu)} \cos 2(\pi \nu - \Delta \psi_x) \beta_x^{\text{mag}} \lambda L \Delta x^{\text{mag}}, \quad (A3)$$

$$\Delta \beta_{y}^{\text{mon}} = \frac{\beta_{y}^{\text{mon}}}{2\sin(\pi \nu)} \cos 2(\pi \nu - \Delta \psi_{y}) \beta_{y}^{\text{mag}} \lambda L \Delta x^{\text{mag}}, \quad (A4)$$

where  $x^{\text{mon}}$  ( $y^{\text{mon}}$ ) is the horizontal (vertical) COD at a BPM,  $x^{\text{mag}}$  ( $y^{\text{mag}}$ ) is the horizontal (vertical) COD at an alignment error magnet,  $\beta_x^{\text{mon}}$  ( $\beta_y^{\text{mon}}$ ) is the horizontal (vertical) beta function at a BPM,  $\beta_x^{\text{mag}}$  ( $\beta_y^{\text{mag}}$ ) is the horizontal (vertical) beta function at an alignment error magnet,  $\Delta \psi_{x,y} \equiv \|\psi_{x,y}^{\text{mon}} - \psi_{x,y}^{\text{mag}}\|$  is the difference in the betatron phase between the magnet and the BPM positions,  $\nu$  is the betatron tune, k is the quadrupole kick,  $\lambda$  is the sextupole kick, and L is the magnet length.

The COD derived from the alignment errors should be converged within the range in which the steering magnets can apply counters. Moreover, optics, such as the beta function, must also be converged within the linear responses. The simulation considering the emittance, tune shift, COD, beta functions, and other optics parameters showed that to substantiate the high-brilliance beam, the net magnet alignment  $1\sigma$  error must be within  $\pm 50~\mu m$ :  $\pm 25~\mu m$  for quadrupole and sextupole magnets on the girder,  $\pm 50~\mu m$  for bending magnet on the girder, and  $\pm 45~\mu m$  for between girders. To realize this, we performed three-step magnet alignments.

First, the magnets were divided into six groups and aligned on six girders (Fig. 26). The magnetic centers for the quadrupole and sextupole magnets were aligned by the vibrating-wire-method (VWM) [39] and fixed on each girder. To monitor the center positions after the VWM alignment, the magnet positions were reflected into base points for laser-tracker measurements. The base points were mounted on top of each magnet and each girder. After this step, the quadrupole and sextupole magnets were well-aligned on each girder, with an accuracy of  $\pm 5~\mu m$  or better. For the bending magnets, we measured the magnetic fields along the mechanical center line with a hole probe. By evaluating the integrated dipole and

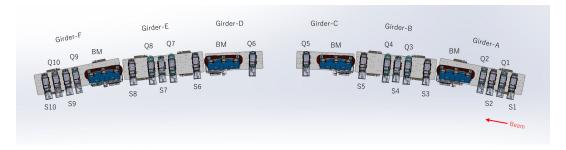


FIG. 26. Magnet girder grouping.

quadrupole fields, the root-mean-square discrepancies from the designed values were found to be 0.09% and 0.18%, respectively. Because of the B-Q combined type bending magnet, the dipole difference can be corrected by horizontal offsetting. We aligned the bending magnets on the girders by applying the offsets, and the maximum was smaller than  $\pm 0.3$  mm. The discrepancy of quadrupole components in the bending magnets was not mechanically corrected during this alignment phase. The differences in dispersion and beta functions from the design as derived from the quadrupole component uncertainty were corrected by the linear optics correction using the beam responses as described in Sec. III G.

Second, in the girder alignment phase with the laser tracker, the girders were mounted on the storage ring floor, and the girder positions were fine tuned. The floor is leveled with epoxy resin to ensure that the surface is flat and to mitigate the vibration transfer from the floor to the girders. Referring to the laser-tracker base points on the floors and the walls of the storage ring tunnel, we evaluated the girder positions, ground levels, and rolls with the laser tracker. The uncertainty of the laser-tracker measurements is approximately 30  $\mu m$  in our configuration, depending on the distances and angles between the magnets and the base points. These works were performed from May to October 2022.

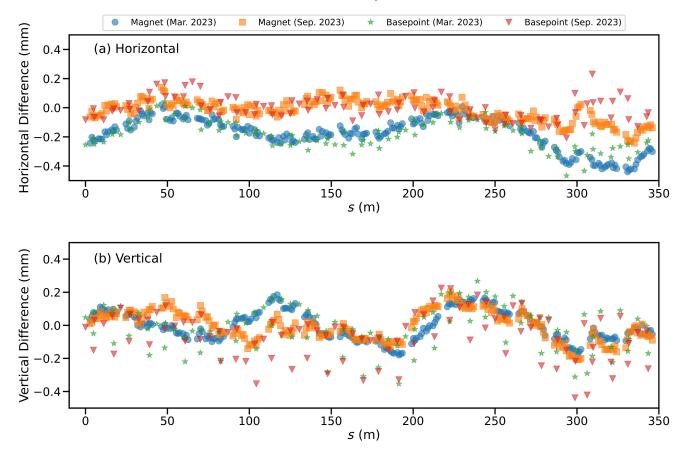


FIG. 27. (a) Horizontal and (b) vertical displacements from the laser-tracker measurement for March (blue and green) and September 2023 (red and orange). The vertical axis in the figure is the difference from the designed position, and the horizontal axis is the path length along the stored beam.

Third, in the confirmation phase in March 2023, we reevaluated all magnet positions with the laser tracker after all the equipment was installed.

Figure 27(a) shows the horizontal displacement from the design, as measured by the laser tracker. The blue circles show the magnet positions measured in March 2023, and sine-curvelike movement is visible. The green stars show the base-point positions, and they also follow the sinelike curve. However, the September 2023 data (orange circles and red stars) show that the displacements are within  $\pm 0.2$  mm. These variations can be explained by the seasonal deformation of the buildings and the grounds. Because the girders are aligned with reference to the floor and wall base points, it is natural for the magnet position variation to obey the base-point seasonal variation.

In Fig. 27(b), the vertical position deviation is stable between March and September 2023, in contrast to the horizontal position deviation. Some base points on the floor are far from the designed positions, but they are also stable seasonally. Because the stability of the buildings and ground influences the stable operation of the storage ring, we plan to continue to perform the laser-tracker measurements regularly.

From the perspective of the stored electron beam, every magnet is on the trajectory of each girder, which is guaranteed by the VWM, even if the girder position is slightly far from the designed circular orbit compared with the buildings. The alignment error problems with the additional kicks mainly arise from the step differences between the girders. Hence, it is essential to prevent additional kicks so that the step-type alignment error is small. Figure 28 shows the relative magnet displacements between the neighborhood girders. Each magnet girder is connected smoothly with  $1\sigma$  within 34 µm (26 µm) in the horizontal (vertical), and this satisfies our requirement of being within 50 µm.

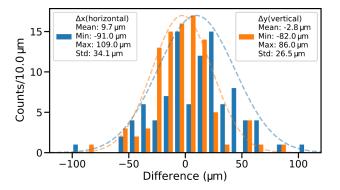


FIG. 28. Relative displacements between the nearest girders from the laser-tracker measurement on March 2023. The histograms of the horizontal and vertical alignment errors are distributed approximately centered.

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