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2D full wave analysis of wave structure by TASK/WF2

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Motivation Formulation Code validation Analysis of wave structure in LATE Summary

1. Motivation

- For spherical tokamak (ST), the use of electron cyclotron heating and current drive (ECH/ECCD) is planned in order to start up plasma and ramp up current without central Ohmic solenoid.
- In the heating and current ramp up process of ST, however, the plasma density becomes higher and we cannot heat the central part of plasma by EC waves due to the wave cutoff.
- Owing to the finite Larmor radius (FLR) effects, the EC waves can be converted into electron Bernstein (EB) waves near the upper hybrid resonance (UHR) layer.
- The EB waves can propagate into higher-density region and heat the central part of plasma.
- Final purpose of this analysis:

quantitative analysis of propagation and absorption of EC and EB waves in a high-density ST

2. Mode conversion

perpendicular XR-mode injection



XL-mode cutoff layer UHR layer XR-mode cutoff layer

Hot Plasma (with FLR effects)



XL-mode cutoff layer UHR layer XR-mode cutoff layer

non-perpendicular O-mode injection



3. High resolution full wave analysis

- For high density STs, full wave analysis is necessary owing to the existence of evanescent layers and mode conversion to EB waves.
- EB wave have very large k_{\perp} (k_{\perp} : the wave number perpendicular to the static magnetic field) and we need high spacial resolution in a 2D plane.
- We have developed the 2D full wave code using finite element method (FEM) with mixed basis functions, TASK/WF2.

4. Formulation for TASK/WF2

- Wave electric field: $\tilde{\boldsymbol{E}}(\boldsymbol{r},t) = \boldsymbol{E}(\boldsymbol{r}) \mathrm{e}^{i\omega t}$
- Used coordinate: Cylindrical coordinate (r, ϕ, z)
- We expand the wave electric field to a Fourier series in the toroidal direction ϕ as

$$\begin{split} \boldsymbol{E}(r,\phi,z) &= \sum_{n_{\phi}=-\infty}^{\infty} \boldsymbol{E}_{n_{\phi}}(r,z) e^{in_{\phi}\phi} \\ &= \sum_{n_{\phi}=-\infty}^{\infty} \{ E_{rn_{\phi}}(r,z) \hat{\boldsymbol{r}} + E_{\phi n_{\phi}}(r,z) \hat{\boldsymbol{\phi}} + E_{zn_{\phi}}(r,z) \hat{\boldsymbol{z}} \} \mathrm{e}^{in_{\phi}\phi}. \end{split}$$

- Boundary condition on the edge of an element:
 - Normal component can be discontinuous.
 - Tangential component is always continuous.
- We use scalar and vector basis functions in order to satisfy the boundary condition.

Scalar basis function



- $N_1 = 1$ on the node 1.
- $N_1 = 0$ on the other nodes.

Vector basis function



- component tangential to the edge 1 is 1 on the edge 1.
- component normal to the edge 2 is 0 on the edge 2.
- component normal to the edge 3 is 0 on the edge 3.
- the magnitude of w_1 is 0 on the node 1.

• Discretization of E(r):

$$\boldsymbol{E}(\boldsymbol{r}) = \left(\sum_{i=1}^{3} E_{\mathrm{p}i} \boldsymbol{w}_{i}(r, z) + \sum_{i=1}^{3} E_{\mathrm{t}i} N_{i}(r, z) \hat{\boldsymbol{\phi}}\right) \mathrm{e}^{i n_{\phi} \phi}$$

 $E_{pi}\;$: the tangential component of \boldsymbol{E} on the edge i

- E_{ti} : the toroidal component of E on the node i
- We consider a particular toroidal mode n_{ϕ} .
- We use weighted residual method and Galarkin's method.
- Weak form of the wave equation:

$$\int_{V} (\nabla \times \boldsymbol{F}) \cdot (\nabla \times \boldsymbol{E}) dV + \int_{S} (\boldsymbol{F} \times \nabla \times \boldsymbol{E}) \cdot \boldsymbol{n} dS$$
$$= \frac{\omega^{2}}{c^{2}} \int_{V} (\boldsymbol{F} \cdot \overleftarrow{\epsilon} \cdot \boldsymbol{E}) dV + i\omega\mu_{0} \int_{V} \boldsymbol{F} \cdot \boldsymbol{J}_{\text{ext}} dV$$

$oldsymbol{F}$:	weight function	
$\stackrel{\leftrightarrow}{\epsilon}$	·	dielectric tensor	

 $oldsymbol{J}_{ ext{ext}}$: external current

5. Mesh



Mesh example: 1261 nodes, 2400 elements

6. Eigenmodes of circular waveguide



• We confirmed that TASK/WF2 can analyze eigenmodes of circular waveguide.

7. Benchmark test with TASK/WM



• TASK/WM and WF2 have different spacial resolution, so there are some differences in their results.

8. Antenna and used parameters

• Antenna

 $r_d = 0.187 {
m m}$

• Used parameters (LATE: Kyoto University)

major radius	R	$0.22\mathrm{m}$
minor radius	a	0.16m
wave frequency	f	5GHz
the number of elements	NEMAX	25350
the ratio of collision frequency to ω	$ u/\omega$	1.0×10^{-3}

• Density profile is parabolic.

 $\theta_2 = -40^{\circ}$

 $\theta_1 = 40^{\circ}$

- Collisional cold plasma model is used for the dielectric tensor.
 - Mode conversion of EC wave into EB wave does not occur.

9. Computational time (one core)



10. Density dependence ($n_{\phi}=0$)

• $B_0 = 0.072 \mathsf{T}$



11. Density dependence ($n_{\phi}=8$)

 $\bullet B_0 = 0.072 \mathsf{T}$



12. Magnetic field dependence





13. Numerical convergence



- Total absorbed power P_{tabs} is used as an index of convergence.
- In the present we use first order element. In order to obtain higher convergence, higher order element is probably required.

14. Summary

- In order to obtain high resolution in poroidal cross section, we have developed 2D full wave code using FEM, TASK/WF2.
- We analyzed eigenmodes of circular waveguide for n_{ϕ} and confirmed that the numerical solution is consistent with the analytic solution.
- We compared EC wave propagation in vacuum analyzed by TASK/WF2 to the one analyzed by TASK/WM and confirmed its conssistency
- We analyzed wave propagation in LATE and presented density dependence and magnetic field dependence of wave propagation.
- Owing to short wavelength wave converted near the UHR layer, numerical solution was not converged for 25000 elements.

• Remaining issues:

- Waveguide excitation
- Formulation and implementation of kinetic dielectric tensor
- Optimization for parallel computing
- Use of higher order element