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Simulation of two-dimensional transport in tokamak plasmas

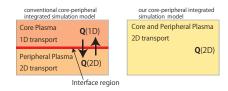
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Background and motivation



• Conventional transport simulation of tokamak plasmas

- In the core of a tokamak plasma transport phenomena have been usually described as one-dimensional problems.
- In the peripheral SOL-divertor plasma, transport phenomena are described as two-dimensional problems

Recent remarkable progress in computational technology has made more consistent two-dimensional transport simulation of tokamak plasmas feasible.

To carry out two-dimensional transport analysis

• Transport model including poloidal-angle dependence is required.

By employing 2D transport model over the entire plasma

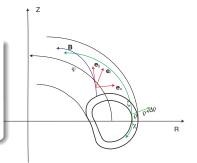
- Analysis of the poloidal angle dependence of the heating efficiency will become available.
- Analysis of the poloidal-angle-dependent transient phenomena will become available.

We formulate an axisymmetric two-dimensional transport modeling which analyzes time evolution of plasmas over the entire tokamak.

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Coordinates

Magnetic Flux Coordinates System (MFCS): $(\xi_1^{M}, \xi_2^{M}, \xi_3^{M}) = (\rho, \chi, \zeta)$ Suitable description of MHD equilibrium configuration



Local Orthogonal Coordinate System (LOCS): $(\xi_1^{L}, \xi_2^{L}, \xi_3^{L}) = (r, \land, \parallel)$

Simpler description on the behavior of magnetized plasmas

Neoclassical Transport Coordinate System (NTCS): $(\xi_1^{\mathbb{N}}, \xi_2^{\mathbb{N}}, \xi_3^{\mathbb{N}}) = (\rho, ||, \zeta)$ Good compatibility with neoclassical theory

Assumptions

- Toroidally axisymmetric plasmas
 - Quantities are independent of the toroidal angle variable
- Quantities related to MHD equilibrium depend only on the flux label
- Relaxation processes much slower than Alfvén time scale
- Weak time dependence of basis vectors
 - Time derivatives of basis vectors are small enough to be ignored

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- Force balance in MHD time scale
 - Force balance in the radial direction is attained in the MHD time scale

Equations to be derived

Transport equations

- Equation for particle density: $n_{\rm e}(
 ho,\chi)$, $n_{\rm i}(
 ho,\chi)$
- Equation for momentum: $n_{\rm e} {m u}_{\rm e}(
 ho,\chi)$, $n_{\rm i} {m u}_{\rm i}(
 ho,\chi)$
- Equation for energy transport: $p_{\rm e}(\rho,\chi)$, $p_{\rm i}(\rho,\chi)$

Electromagnetic equations

- Poisson equation for electrostatic potential: $\phi(\rho)$
- Magnetic diffusion equation: $\iota(\rho)$
- Grad-Shafranov equation: $\psi(R,Z)$

Braginskii's equations

Two-fluid transport equation for cold plasma.

• Equation of continuity

$$\frac{\partial n_a}{\partial t} + \nabla \cdot (n_a \boldsymbol{u}_a) = S_a$$

• Equation of motion

$$\frac{\partial}{\partial t} (m_a n_a \boldsymbol{u}_a) = -\nabla \cdot (m_a n_a \boldsymbol{u}_a \boldsymbol{u}_a) - \nabla p_a - \nabla \cdot \stackrel{\leftrightarrow}{\pi}_a + e_a n_a (\boldsymbol{E} + \boldsymbol{u}_a \times \boldsymbol{B}) + \boldsymbol{R}_a + m_a S_{u_a} \boldsymbol{u}_a$$

• Equation for energy

$$\frac{3}{2}\frac{\partial p_a}{\partial t} + \nabla \cdot \left(\boldsymbol{q}_a + \frac{5}{2}p_a\boldsymbol{u}_a\right) = -\overset{\leftrightarrow}{\pi}_a : \nabla \boldsymbol{u}_a + \boldsymbol{u}_a \cdot \nabla p_a + Q_a + S_{p_a}$$

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Formulation of transport equations

• Policy for the derivation of transport equations

- For compatibility with the neoclassical transport theory, three components of vector quantities are represented by NTCS.
- Spatial independent variables are expressed in MFCS
- Neoclassical viscosity tensor in LOCS

$$\overset{\leftrightarrow}{\pi}_{a} \equiv 3 \frac{\boldsymbol{u}_{a} \cdot \nabla \chi}{\boldsymbol{B} \cdot \nabla \chi} \nabla_{\parallel} B \left(\frac{1}{3} \sum_{i=1}^{3} \boldsymbol{e}_{\xi_{i}^{\perp}} \boldsymbol{e}_{\xi_{i}^{\perp}} - \boldsymbol{e}_{\parallel} \boldsymbol{e}_{\parallel} \right)$$

• The equation for particle density

$$\frac{\partial n_a}{\partial t} + \sum_{i=1}^3 \sum_{j=1}^3 \frac{1}{\sqrt{g}} \frac{\partial}{\partial \xi_i^{\mathsf{M}}} (\sqrt{g} n_a \mathcal{T}_{ij}^{\mathsf{MN}} u_a^{\xi_j^{\mathsf{N}}}) = S_a$$

where T_{ij}^{MN} is the transformation matrix from MFCS to NTCS.

• Equation for momentum

$$\begin{split} \frac{\partial}{\partial t} \left(m_a n_a \boldsymbol{u}_a \right) &= -\sum_{i=1}^3 F_a^{\mathrm{kin},i} \boldsymbol{e}_{\boldsymbol{\xi}_i^{\mathrm{M}}} - \nabla p_a \\ &- \frac{1}{3} \nabla N_a^{\mathrm{neo}} + \nabla_{\parallel} N_a^{\mathrm{neo}} - N_a^{\mathrm{neo}} \nabla_{\parallel} \ln B + N_a^{\mathrm{neo}} \boldsymbol{\kappa} \\ &+ e_a n_a \left(\boldsymbol{E} + \boldsymbol{u}_a \times \boldsymbol{B} \right) + \boldsymbol{R}_a + m_a S_{u_a} \boldsymbol{u}_a \end{split}$$

where, $F_a^{\text{kin},i}$ is the contravariant component of kinetic force in MFCS and N_a^{neo} the parallel coefficient of neoclassical viscosity.

The equation for momentum in each direction of NTCS is derived by taking the scalar product with $e^{\xi_i^N}$.

$$e^{\xi_1^{\mathsf{N}}} \equiv \nabla \rho, \quad e^{\xi_2^{\mathsf{N}}} \equiv e_{\parallel}, \quad e^{\xi_3^{\mathsf{N}}} \equiv \nabla \zeta$$

• Equation for momentum in radial direction

$$\begin{split} 0 &= -F_a^{\mathrm{kin},1} - \sum_{i=1}^3 g^{1i} \frac{\partial p_a}{\partial \xi_i^{\mathrm{M}}} - \sum_{i=1}^3 \frac{1}{3} g^{1i} \frac{\partial N_a^{\mathrm{neo}}}{\partial \xi_i^{\mathrm{M}}} + N_a^{\mathrm{neo}} \kappa^{\rho} \\ &- g^{11} e_a n_a \frac{\partial \phi}{\partial \rho} + e_a n_a \hat{E}^{\rho} + \sum_{i=1}^3 C_a^{\mathrm{Lor},i} n_a u_a^{\xi_i^{\mathrm{N}}} + R_a^{\rho} + m_a S_a u_{u_a}^{\rho} \end{split}$$

where $C_a^{{\rm Lor},i}$ and R_a^ρ are the coefficient of the Lorentz force term and the contravariant radial friction force

$$\begin{split} C_a^{\mathrm{Lor},1} &= 0, \quad C_a^{\mathrm{Lor},2} = \frac{e_a BI}{\psi'}, \quad C_a^{\mathrm{Lor},3} = -\frac{e_a B^2 R^2}{\psi'} \\ R_a^{\rho} &\equiv \mp \frac{m_{\mathrm{e}} n_{\mathrm{e}}}{\tau_{\mathrm{e}}} u^{\rho} \mp \frac{3}{2\tau_{\mathrm{e}} \Omega_{\mathrm{e}}} \frac{I}{\sqrt{g} B} n_{\mathrm{e}} \frac{\partial T_{\mathrm{e}}}{\partial \chi} \end{split}$$

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• Equation for momentum in parallel direction

$$\begin{split} \frac{\partial}{\partial t} \left(m_a n_a u_{a\parallel} \right) &= -\sum_{i=1}^{3} C_a^{\mathrm{kin},i} F_a^{\mathrm{kin},i} - \frac{\psi'}{\sqrt{gB}} \frac{\partial p_a}{\partial \chi} \\ &- \frac{\psi'}{\sqrt{gB}} N_a^{\mathrm{neo}} \frac{\partial \ln B}{\partial \chi} + \frac{2}{3} \frac{\psi'}{\sqrt{gB}} \frac{\partial N_a^{\mathrm{neo}}}{\partial \chi} \\ &+ e_a n_a \hat{E}_{\parallel} + R_{a\parallel} + m_a S_{u_a} u_{a\parallel} \end{split}$$

where $C_a^{\rm kin,i}$ and $R_{a\parallel}$ are the coefficient of kinetic stress force in each direction and the parallel friction force

$$\begin{split} C_a^{\mathrm{kin},1} &= \frac{\psi' g_{21}}{\sqrt{g}B}, \quad C_a^{\mathrm{kin},2} &= \frac{\psi' g_{22}}{\sqrt{g}B}, \quad C_a^{\mathrm{kin},3} &= \frac{I}{B} \\ R_{a\parallel} &\equiv \mp \left\{ 0.51 \frac{m_{\mathrm{e}} n_{\mathrm{e}}}{\tau_{\mathrm{e}}} \left(u_{\mathrm{e\parallel}} - u_{\mathrm{i}\parallel} \right) + 0.71 \frac{\psi'}{\sqrt{g}B} n_{\mathrm{e}} \frac{\partial T_{\mathrm{e}}}{\partial \chi} \right\} \end{split}$$

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• Equation for momentum in toroidal direction

$$\begin{split} \frac{\partial}{\partial t} \left(m_a n_a u_a^{\zeta} \right) &= -F_a^{\mathrm{kin},3} \\ &- \frac{I\psi'}{\sqrt{g}B^2R^2} N_a^{\mathrm{neo}} \frac{\partial \ln B}{\partial \chi} + \frac{I\psi'}{\sqrt{g}B^2R^2} \frac{\partial N_a^{\mathrm{neo}}}{\partial \chi} + N_a^{\mathrm{neo}} \kappa^{\zeta} \\ &+ e_a n_a \hat{E}^{\zeta} + \frac{e_a \psi'}{R^2} n_a u_a^{\rho} + R_a^{\zeta} + m_a S_{u_a} u_a^{\zeta} \end{split}$$

where R_a^{ζ} is the contravariant toroidal friction force

$$R_{a}^{\zeta} \equiv \mp \frac{m_{\rm e}n_{\rm e}}{\tau_{\rm e}} \left\{ \left(u_{\rm e}^{\zeta} - u_{\rm i}^{\zeta} \right) - 0.49 \frac{I}{BR^{2}} \left(u_{\rm e\parallel} - u_{\rm i\parallel} \right) \right\}$$
$$\mp 0.71 \frac{\psi' I}{\sqrt{g}B^{2}R^{2}} n_{\rm e} \frac{\partial T_{\rm e}}{\partial \chi} \mp \sum_{i=1}^{3} \frac{3}{2\tau_{\rm e}\Omega_{\rm e}} \frac{\psi' g^{1i}}{BR^{2}} n_{\rm e} \frac{\partial T_{\rm e}}{\partial \xi_{i}^{\rm M}}$$

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Equation for internal energy is obtained by transforming equation for energy transport of Braginskii's equation into the advection-diffusion form

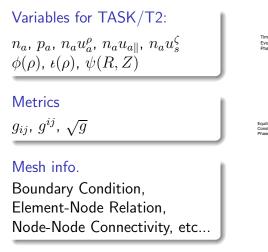
• Equation for internal energy

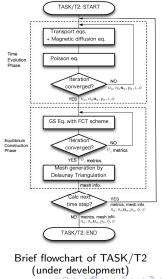
$$\frac{\partial}{\partial t} \left(\frac{3}{2} p_a\right) + \nabla \cdot \left(p_a \boldsymbol{u}_{p_a} - n_a \overleftrightarrow{\chi}_a \cdot \nabla T_a\right) = Q_{p_a}$$

where $\boldsymbol{u}_{p_a} \equiv (5/2)\boldsymbol{u}_a + p_a^{-1}\boldsymbol{q}_{u_a}$, Q_{p_a} and $\overset{\leftrightarrow}{\chi}_a$ are the the energy flow velocity, the energy source term and the diffusion coefficient tensor and respectively.

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Current program design





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Current status and issues of TASK/T2: TE-phase

Employed algorithms

- Discretization:
 - SUPG-FEM: Transport eqs.
 - BG-FEM: Magnetic diffusion eq. and Poisson eq.
- Element: Multi-scale rectangular element
- Matrix Solver: Krylov subspace iterative method (PETSc library)
- Nonlinear Solver: Picard iteration

We have derived transport eqs. and been coding TE-Phase; however, there are still remains some issues in transport modeling.

- Appropriate modeling of gyro-viscous force in core region
- Appropriate energy cancellation between diamagnetic terms

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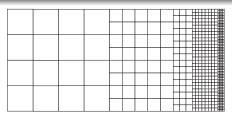
Current status and issues of TASK/T2: EC-phase

Grad-Shafranov Eq. with FCT scheme

- TASK/EQU
 - Free boundary 2D MHD equilibrium solver with FCT scheme included in integrated toroidal plasma modeling code TASK.

Mesh generation

• Multi-scale structural rectangular mesh generation algorithm



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Summary and Future works

Summary

- A set of equations required for two-dimensional transport modeling for tokamak plasmas has been derived for integrated analysis of core and peripheral plasmas
 - Transport equations are derived from Braginskii's equations with the neoclassical viscosity in MFCS and reduced to two-dimensional with toroidal axisymmetry.
 - By combining these transport equations with the electromagnetic equations, a more self-consistent two-dimensional transport analysis including the field evolution will be available.

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Future works

- Developing the two-dimensional transport code using the FEM to simulate time evolution of tokamak plasmas.
 - Analysis of the asymmetric effect in limiter configuration
 - Full 2D transport analysis in entire tokamak plasma