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Simulation study of L/H transition with self-consistent integrated modelling of core and SOL/Divertor transport

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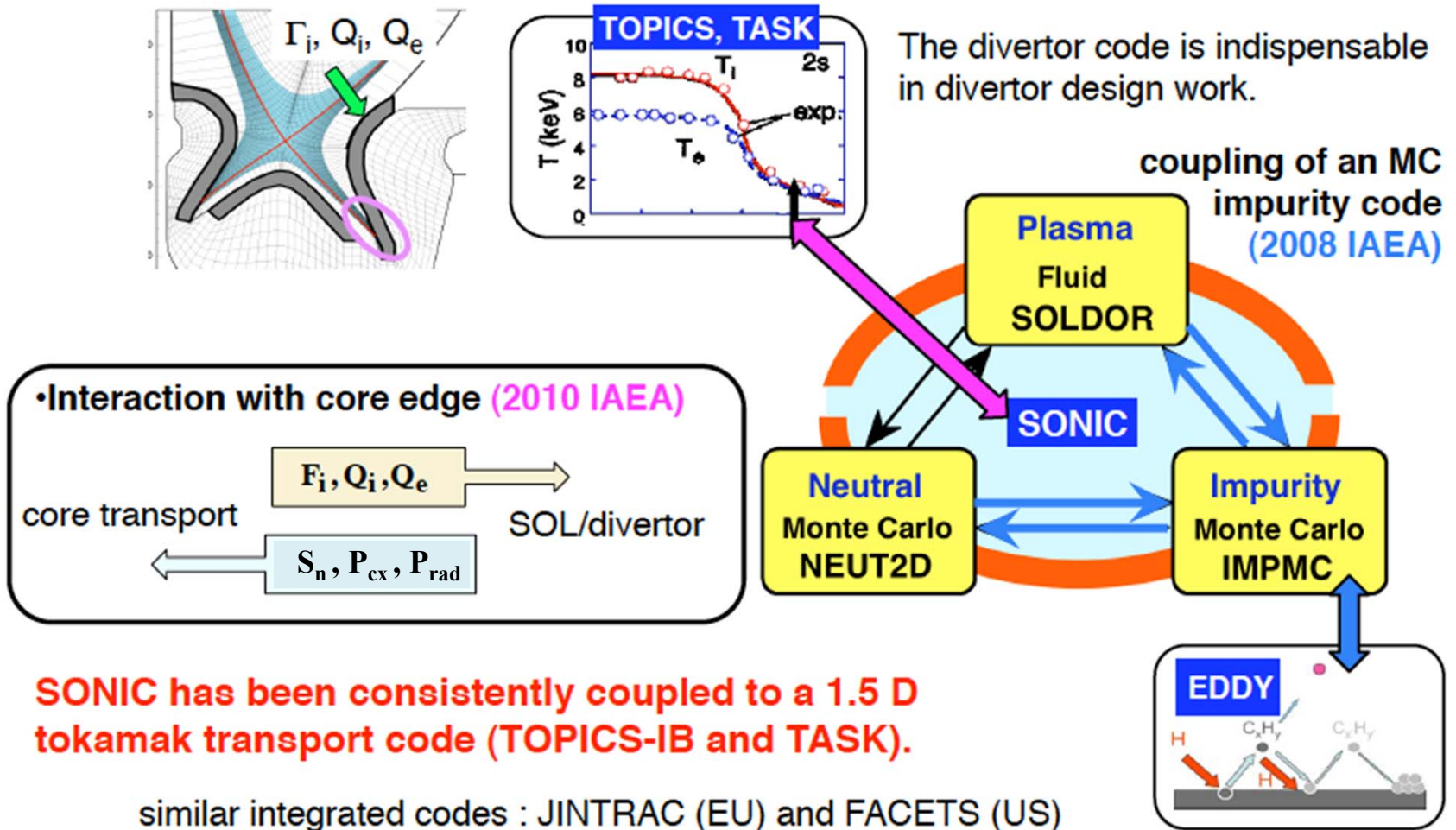
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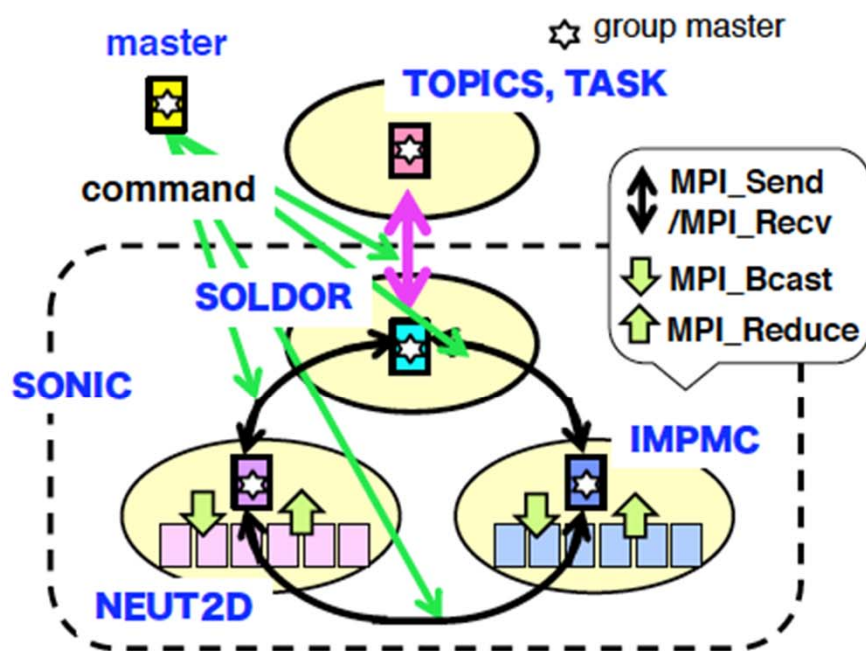
Integrated Divertor Code "SONIC"



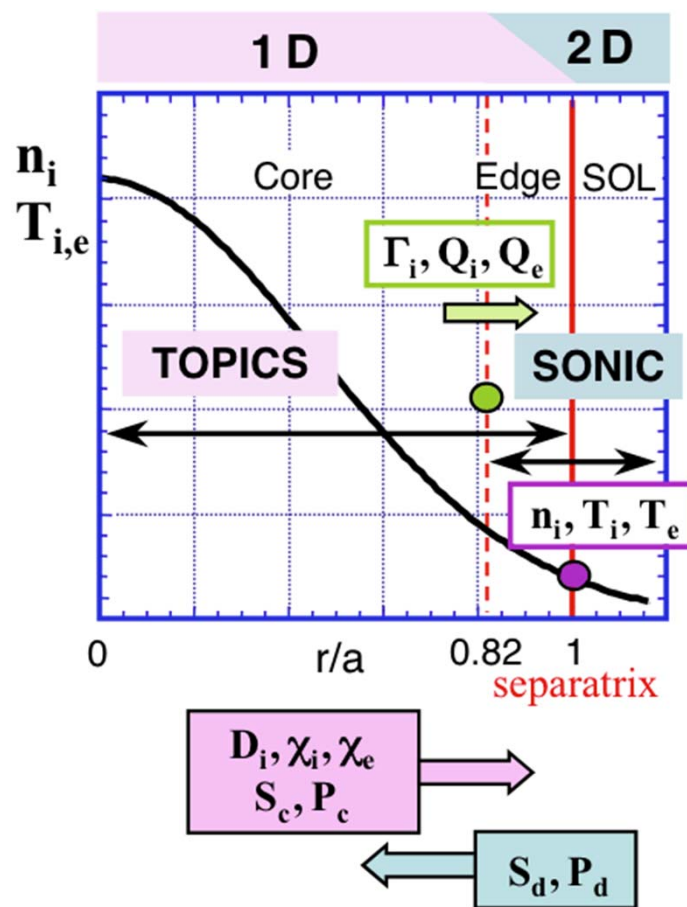
Coupling to the Core Transport Code

New MPMD parallel computing System

enables unification of independently established code suite efficiently.



Relation between TOPICS and SONIC



Data exchange in every 200 μ s

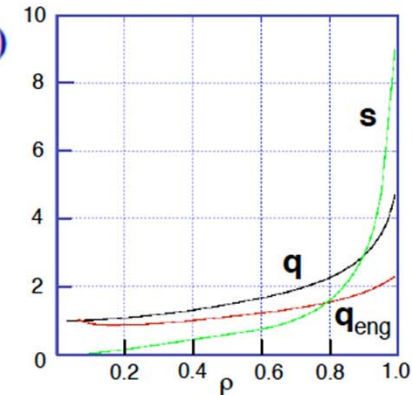
Tuned CDBM Model

$$\chi_{\text{CDBM}} = \frac{c^2}{\omega_{pe}^2} \frac{v_A}{qR} |\alpha|^{3/2} F(s, \alpha), \quad \alpha = -q^2 R \frac{d\beta}{dr} \quad (\text{K. Itoh et al., PPCF, 1994})$$

■ At the edge, $\chi \approx \frac{q^3(1)}{s^{1/2}}$ can not decrease due to large $q(1)$

✓ **Modification (I)** Using Engineering q

$$q(r) \equiv q_{\text{eng}}(r) = \frac{2\pi k r^2 B_t}{\mu_0 R I(r)}$$

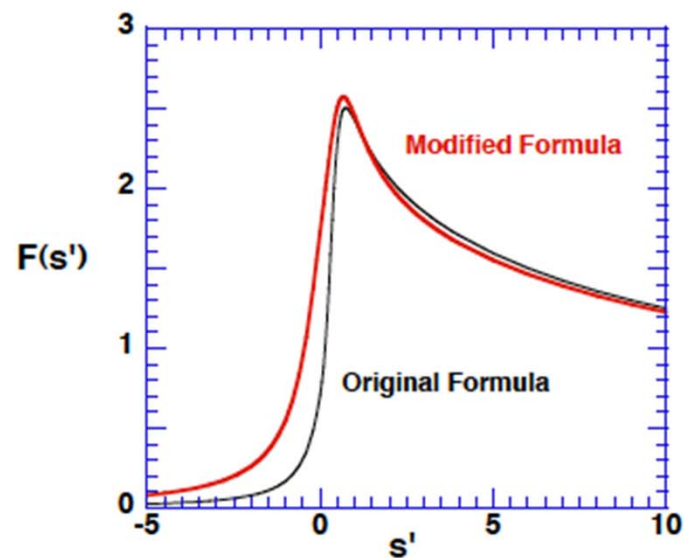


■ In the weak-shear central region, F is very small and the ITB can be easily formed by the heating power smaller than an ETB threshold (L-H transition).

✓ **Modification (II)** Moderate decrease of F for $s' < 0$ regime

$$F(s, \alpha) \equiv F(s') = \begin{cases} \sqrt{3}(1 + 2s'^{2.5}) / (1 - s' + 1.35s'^2 + 0.7698s'^3), & s' > 0 \\ \sqrt{3} / [(1 - s')(1 - s' + 3s'^2)]^{1/2}, & s' < 0 \end{cases} \quad s' \equiv s - \alpha$$

Tuned CDBM Model (Cont.)



■ In the weak-shear central region, $(\omega_{\text{EXB}}/\gamma_{\text{CDBM}})$ becomes very small and the ITB can be easily formed before the L-H transition.

✓ **Modification (III)** Modification of shear dependence on γ_{CDBM}

$$\gamma_{\text{CDBM}} = |\alpha|^{1/2} \frac{v_A}{qR} F(s') \quad (\text{J.W. Connor, PPCF 1993})$$

Tuned CDBM Model (Cont.)

Transport Model $\chi_{\text{ANO}} = \frac{A\chi_{\text{CDBM}}}{1+(B\omega_{\text{EXB}}/\gamma_{\text{CDBM}})^K}$ **(T. S. Hahm and K.H. Burrell, PoP 1995)**

✓ Adjustment of Transport Coefficients

$$\omega_{\text{EXB}} = (RB_{\theta}/B_t) |d/dr (E_r/RB_{\theta})| - dp_i/dr + e n_i E_r = 0$$

A: $HH \approx 0.5$ for L-mode

B: L-mode for $P_{\text{loss}} < P_{\text{LH}}$

K: $\omega_{\text{EXB}} \sim |\alpha|$, $\gamma_{\text{CDBM}} \sim |\alpha|^{1/2}$, $\chi_{\text{CDBM}} \sim |\alpha|^{3/2}$

$$\chi_{\text{ANO}} \sim \frac{|\alpha|^{3/2}}{1+C|\alpha|^{K/2}} \quad K \rightarrow 3 \quad (\text{Note that } K=4 \text{ is numerically difficult})$$

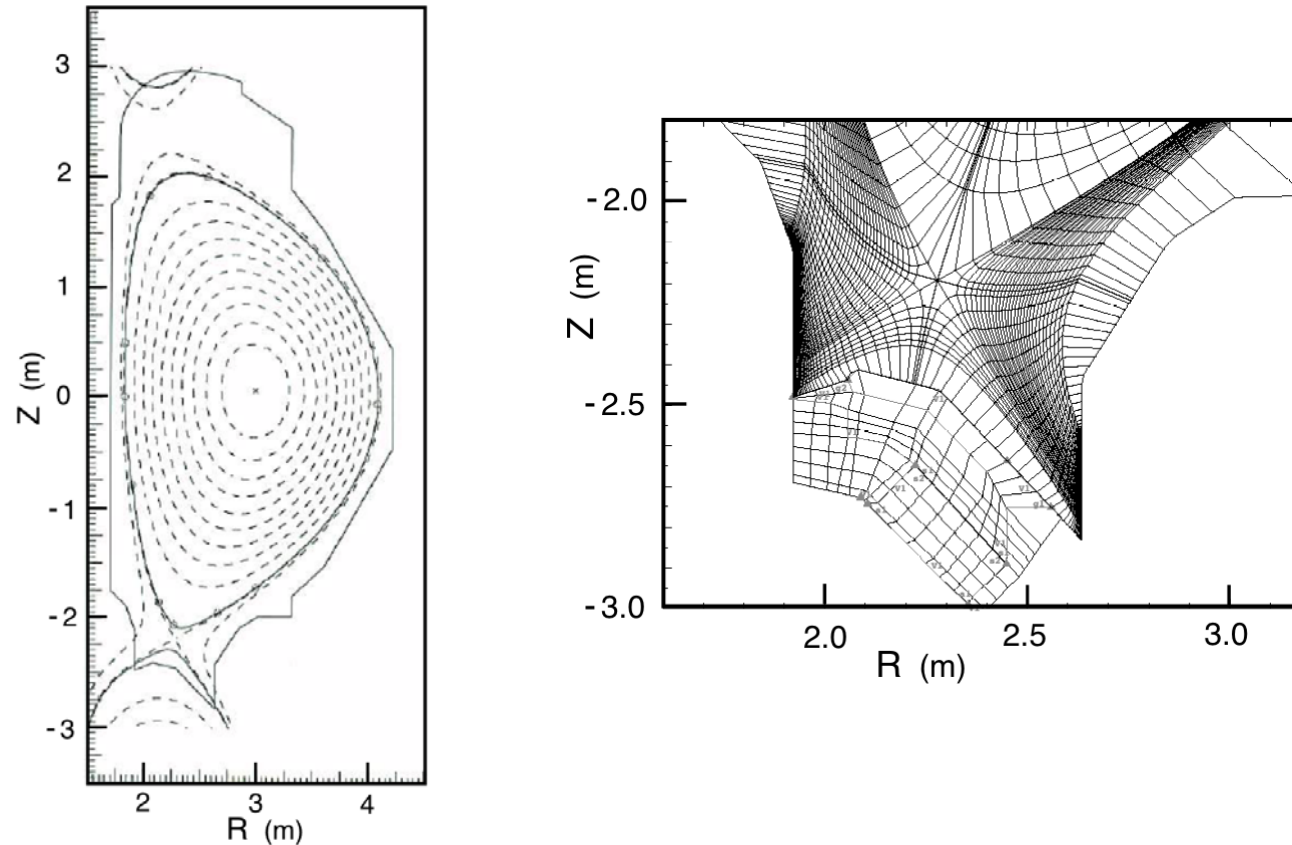
$$P_{\text{LH}} = 0.06(B_t n_{20})^{0.7} S^{0.9} \text{ (MW, T, } 10^{20} \text{m}^{-3}, \text{m}^2) \quad (\text{T. Takizuka, PPCF 2004})$$

For JT60-SA with

$$B_t = 2.3\text{T}, n_{20} = 0.3 \times 10^{20} \text{m}^{-3} \quad (n_{\text{GW}} = 1 \times 10^{20} \text{m}^{-3} \text{ for } I_p = 4\text{MA}, a = 1.13\text{m}), S = 190\text{m}^2$$

$$P_{\text{LH}} \rightarrow 5\text{MW}$$

MHD Equilibrium of JT60-SA



MHD equilibrium of a JT-60SA plasma with single-null divertor configuration. $R = 3$ m, $a = 1.1$ m, $\beta = 1.8$, $\beta_p = 0.55$, $I_p = 4$ MA, and $B_t = 2.3$ T. 2D mesh configuration for SONIC is also shown.

Scenario of Transport Simulation

(1) Weak heating L-mode Phase

$P_{\text{NB}} = 0.5$ MW is added to a plasma with $I_p = 4$ MA and $B_t = 2.3$ T.

A slightly-broad current density profile $j(r)$ is given ($l_i = 0.7$).

Effective charge number $Z_{\text{eff}} = 2$ is set uniformly.

Ohmic heating power P_{OH} is calculated as 3.1 MW.

Radiation power from the core plasma is set $P_{\text{rad}} = 1$ MW.

Line average electron density is $\bar{n}_e \sim 0.25 \times 10^{20} \text{m}^{-3}$.

The HH factor by the IPB98(y,2) standard is calculated as ~ 0.5 .

(2) NB Phase

NB heating is suddenly increased up to $P_{\text{NB}} = 8$ MW at $t = 3$ s.

(3) L/H Transition Phase

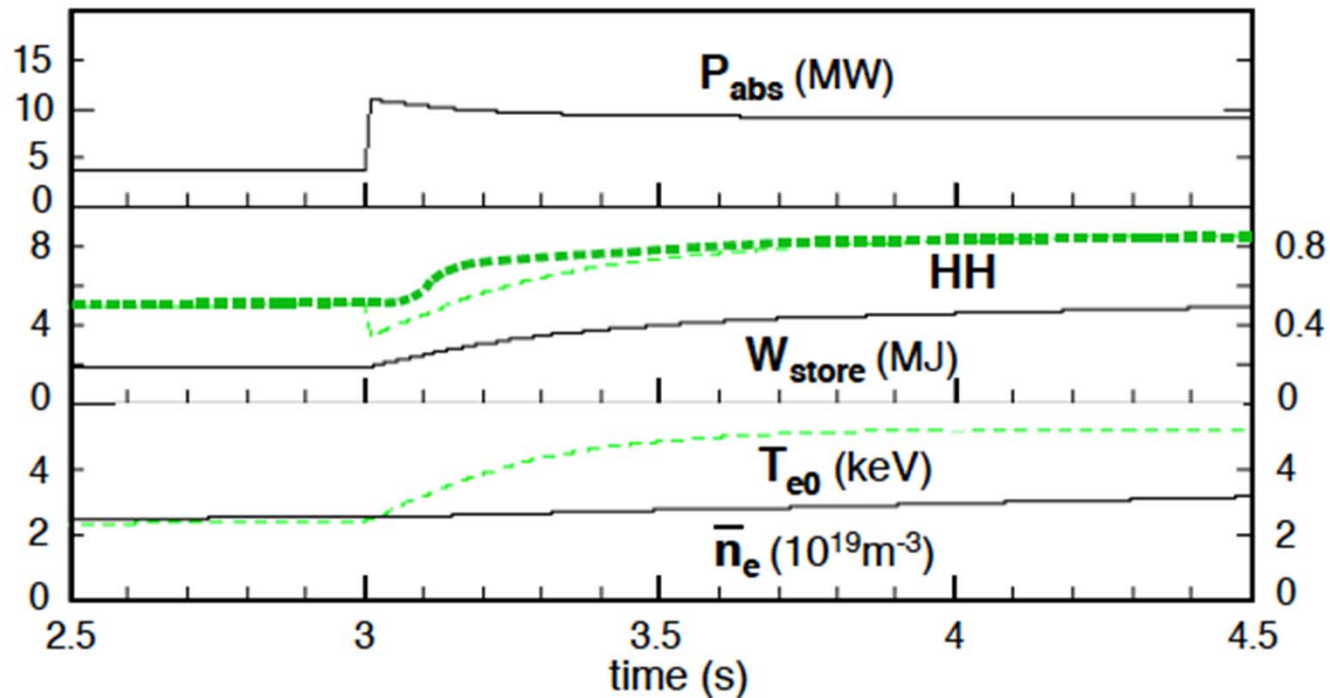
An L/H transition occurs self-consistently within the present transport model.

Absorbed power at this time, $t \approx 3.1$ s, is 10.4 MW including $P_{OH} = 2.4$ MW. Time variation of the store energy $dW/dt = 5.6$ MW.

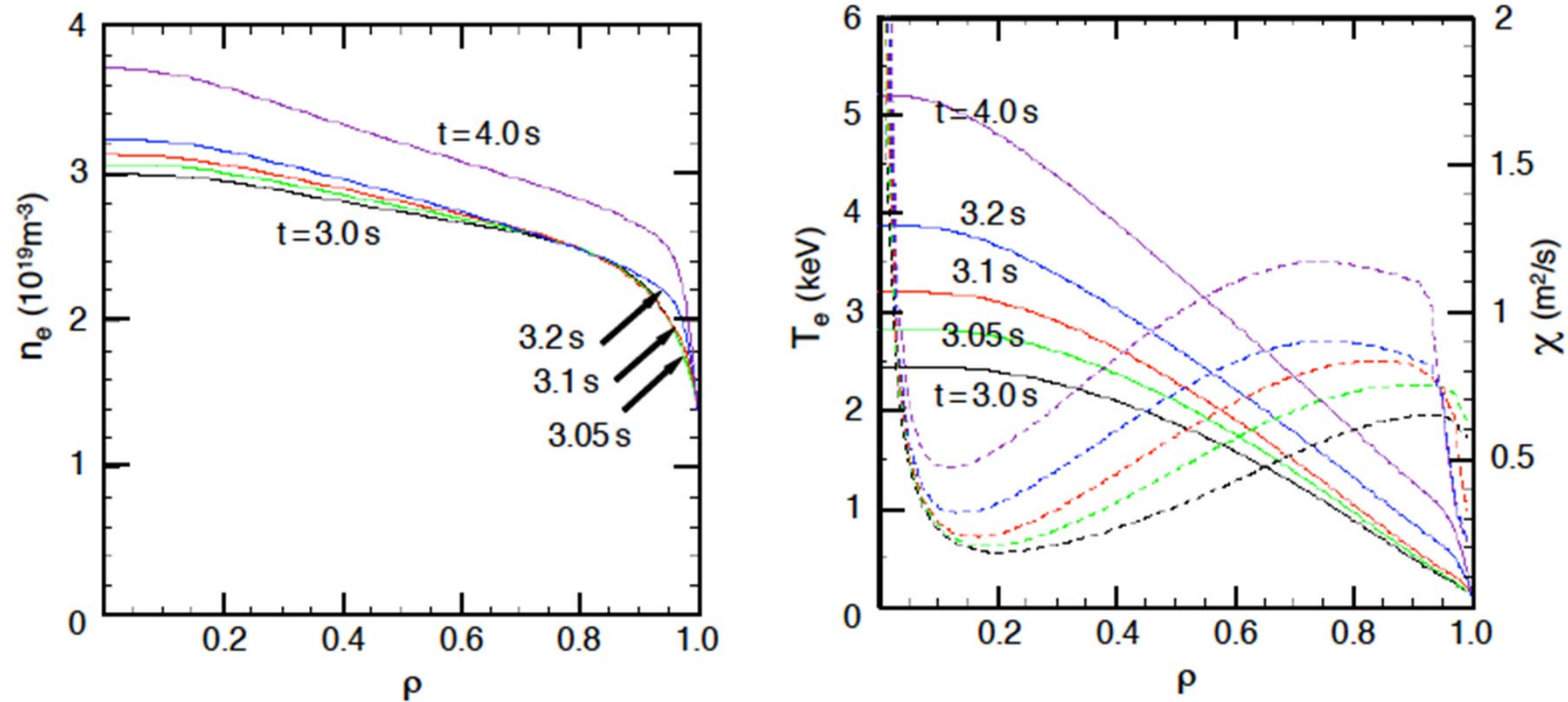
The loss power is estimated as 4.8 MW, which is similar to P_{thr} predicted by the threshold power scaling.

(4) H-mode Phase

The HH factor becomes about 0.85 in the H-mode phase.

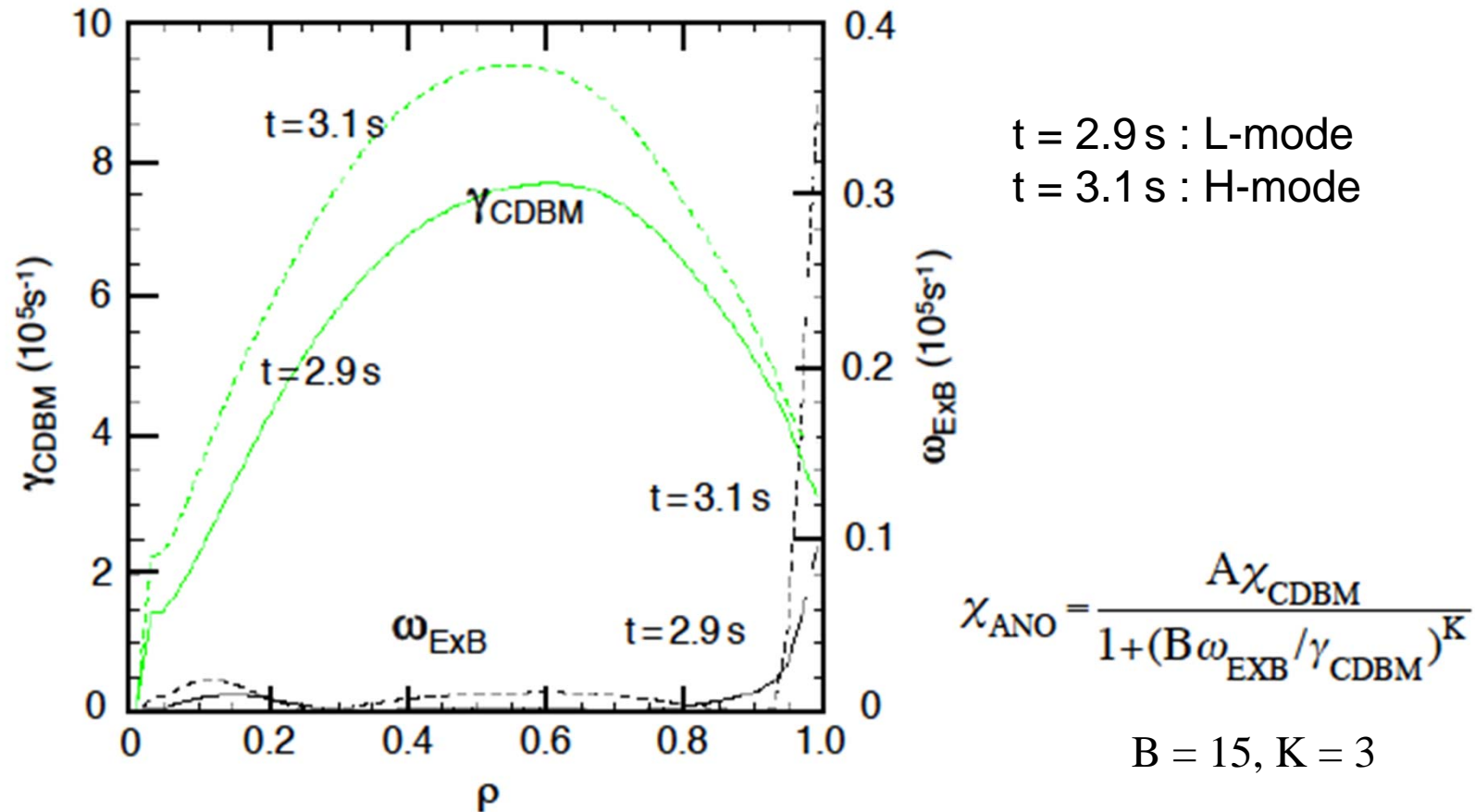


Time Evolution of Density and Temperature in L/H Transition Phase



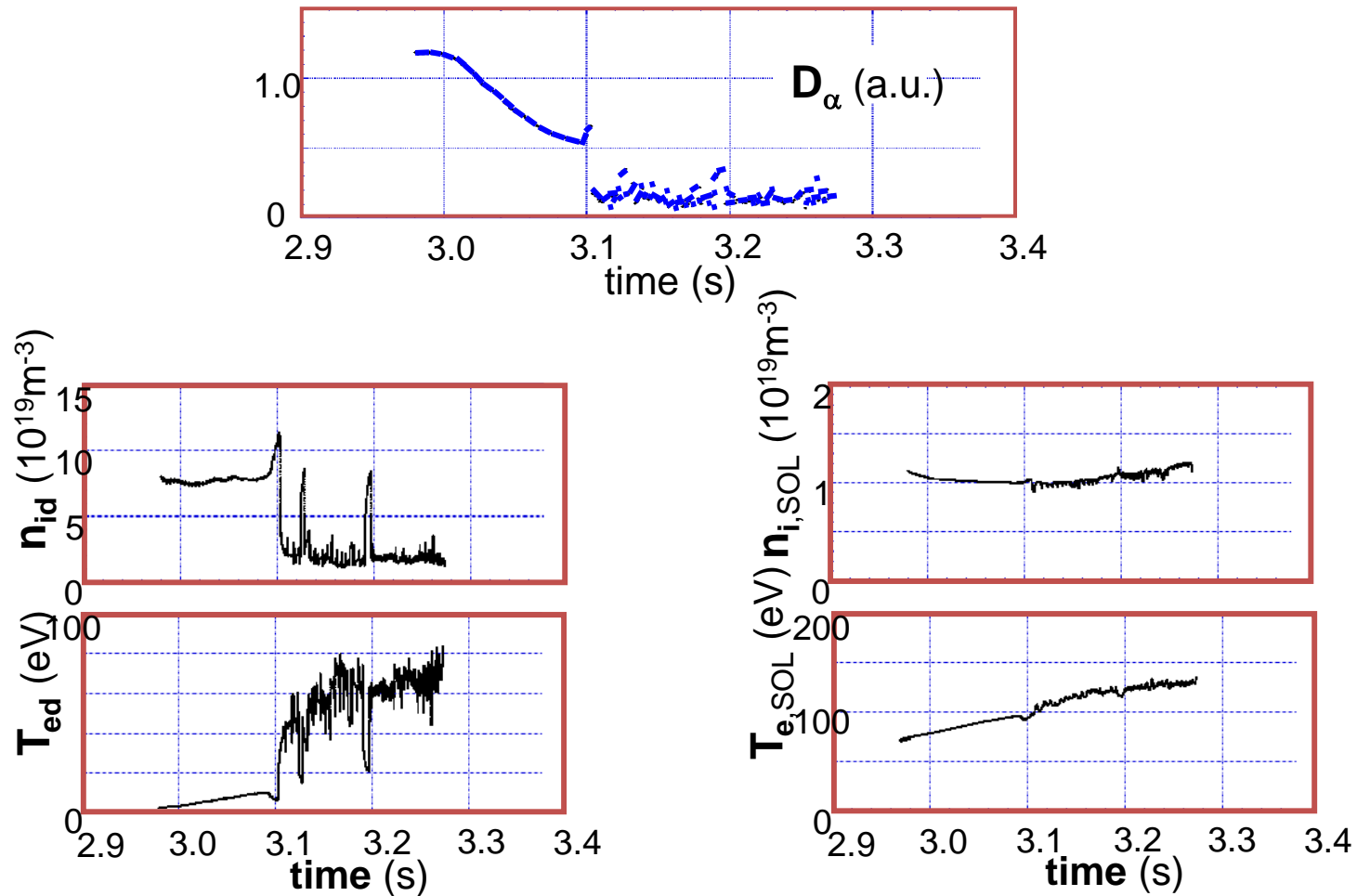
Evolution of electron density profile $n_e(r)$, electron temperature profile $T_e(r)$, and heat diffusivity profile $\chi(r)$. NB heating power is increased to 8 MW from the time $t = 3 \text{ s}$. An L/H transition occurs around $t = 3.1 \text{ s}$. χ is drastically dropped in the edge region and the pedestals are clearly formed on n_e and T_e profiles.

Turbulence Suppression by ExB Shearing Rate



After L/H transition, ExB shearing rate increment clearly overcomes the CDBM growth rate increment at the edge region.

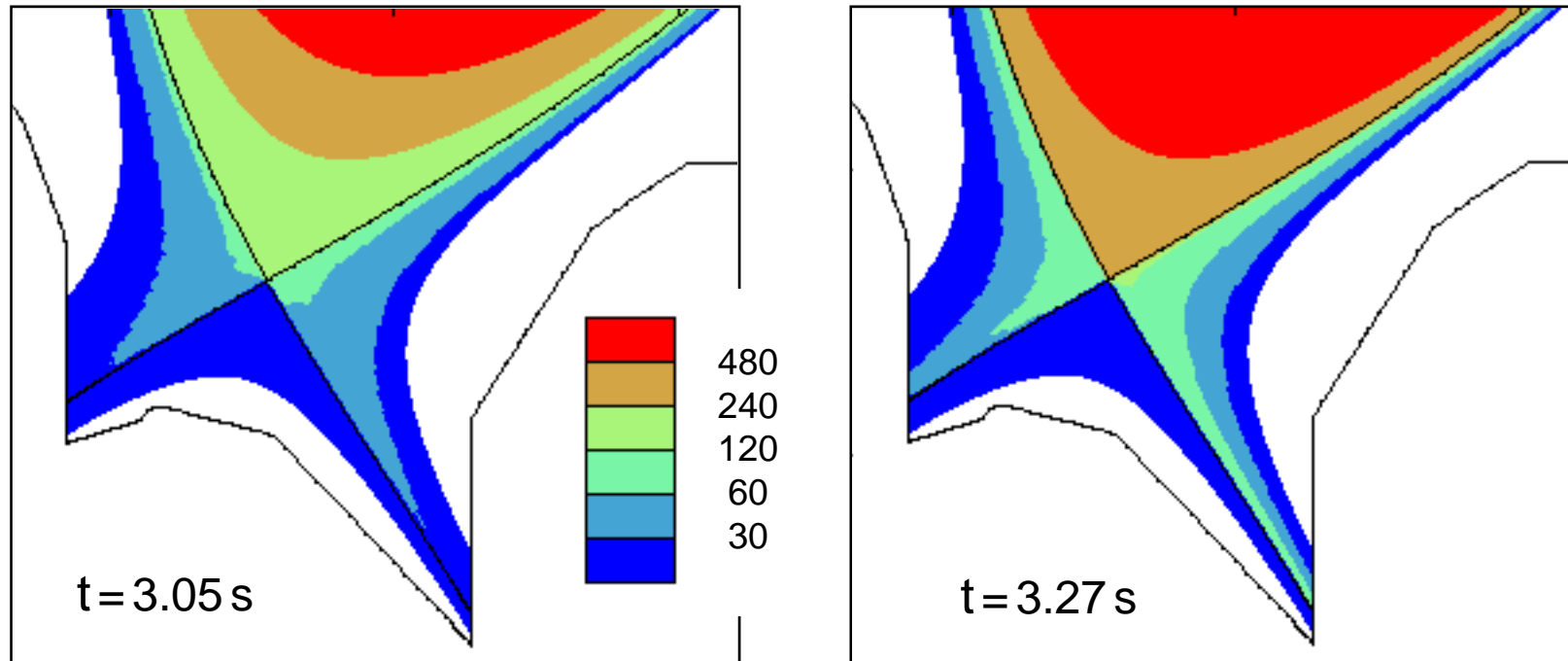
Time evolution of D_α and Profiles by SONIC



Time evolution of electron density and temperature (n_{id} , T_{ed}) at outer divertor strike point and ($n_{i,SOL}$, $T_{e,SOL}$) at outer mid-plane through the L/H transition.

Temporal fluctuation of SOL/divertor-plasma is observed in H-mode phase.

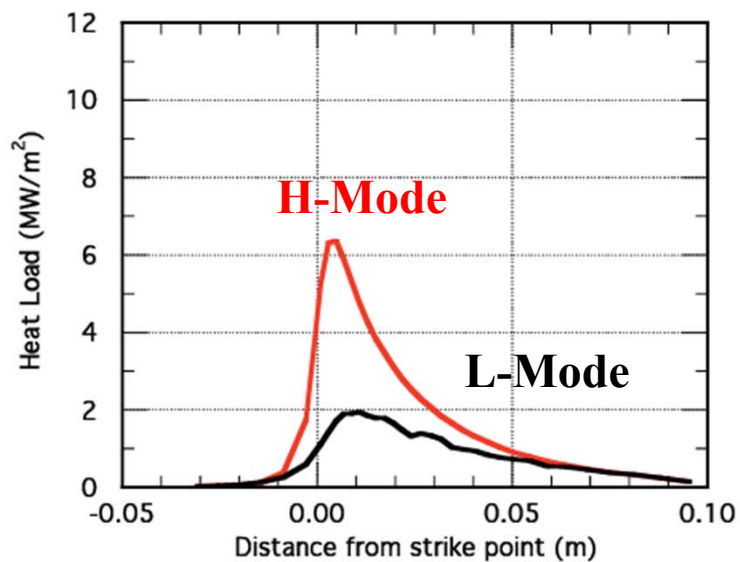
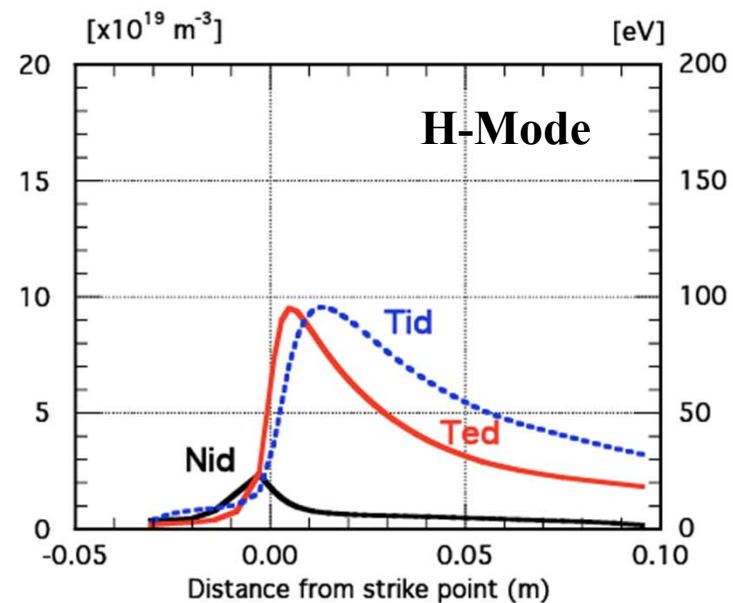
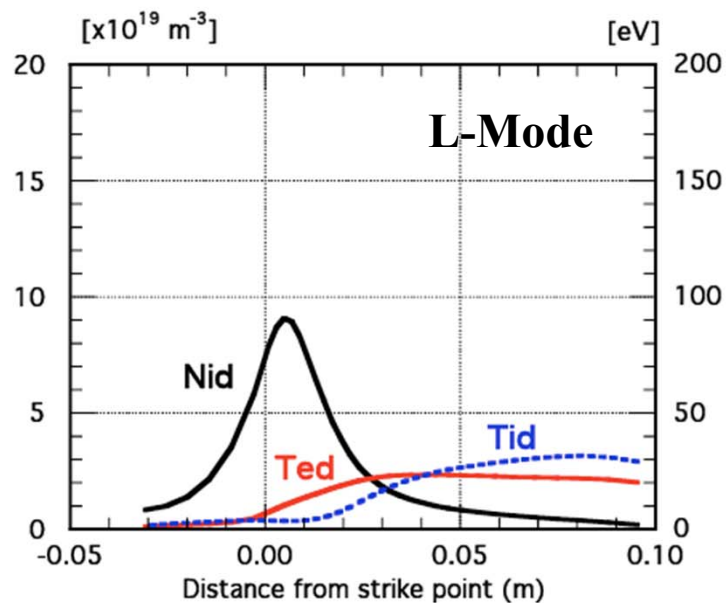
2D electron temperature before and after the L/H transition



After transition, electron temperature increases near divertor plate.

T_{ed} increases from $\sim 10 \text{ eV}$ to $\sim 50 \text{ eV}$.

Heat Load on Outer Divertor Plate



Summary

Self-consistent integrated modelling of core and SOL/divertor transport (TOPICS-IB & SONIC) is developed by MPMD parallel computing system.

The dynamic simulation for the L/H transition in JT-60SA is carried out by integrated code with tuned CDBM transport model including the $E \times B$ shearing effect.

Impacts of SOL/divertor transport on the L/H transition are studied. It is found that after the transition, the electron density suddenly drops and the electron temperature increases near the divertor plate. The temporal fluctuation of the SOL plasma is observed in the H-mode phase.

Examination of the numerical accuracy and analyses on the physical mechanisms are left for future work.