

Fokker-Planck Simulation of the Runaway Electron Generation in Tokamak Disruption

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Introduction (RE generation)

- The importance of the Runaway Electron (RE) generation study during tokamak disruption:
 - Thermal quench due to tokamak disruption induces strong toroidal electric field.
 - Because of the low collisionality for high velocity, some of electrons are accelerated to relativistic high energy.
 - The impact to the first wall leads crucial localized heat load.
 - To avoid this, several mitigation methods are developed.
- The estimation of the amount of REs during tokamak disruption is required for the development of the operation scenarios.

Introduction (hot-tail effect)

- Non-thermal effect should be included for RE gen. simulation
 - If the thermal quench is enough short, the plasma cools down so quickly that high velocity electrons do not have enough time to thermalize.
 - The rapid cooling forms the high velocity tail of the electron velocity distribution.
 - This tail enhances the primary RE generation and this effect is called as hot-tail effect.
 - Since the mitigation, such as Massive Gas Injection (MGI), makes the thermal quench time to be short, the estimation of the hot-tail effect is important for ITER.
- In order to include the hot-tail effect to RE generation simulation, we have developed a Fokker-Planck code TASK/FP.

Simulation Code: TASK/FP

- TASK/FP is a Fokker-Planck code to calculate the time evolution of momentum distribution function f in 3 dimension : (p, θ, ρ) .

Fokker-Planck equation in (p, θ, ρ) coordinate

$$\frac{\partial f_s}{\partial t} = -\nabla_{p,\rho} \cdot \mathbf{S} = -\frac{1}{p^2} \frac{\partial}{\partial p} p^2 S_p - \frac{1}{p \sin \theta} \frac{\partial}{\partial \theta} \sin \theta S_\theta - \frac{1}{\rho} \frac{\partial}{\partial \rho} \rho S_\rho$$

Elements of flux

$$S_p = -D_{pp} \frac{\partial f}{\partial p} - D_{p\theta} \frac{1}{p} \frac{\partial f}{\partial \theta} + F_{\rho} f$$

$$S_\theta = -D_{\theta p} \frac{\partial f}{\partial p} - D_{\theta\theta} \frac{1}{p} \frac{\partial f}{\partial \theta} + F_{\theta} f, \quad S_\rho = -D_\rho \frac{\partial f}{\partial \rho} + F_\rho f$$

Equations 1: E field

- The induced electric field obeys:

1. Diffusion equation of E field

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial E}{\partial r} \right) = \mu_0 \frac{\partial j}{\partial t}$$

- Ohm's law is adopted as a closure.

2. Ohm's law (n_r : REs density, σ_{sp} : Spitzer conductivity)

$$j = \sigma_{sp} E + e c n_r$$

- This equation assumes
 - The velocity of all REs equals to that of light.
 - All of REs are collisionless.

Equations 2: RE gen. rate

- There are two kind of RE generation mechanisms, primary and secondary.
 - The primary RE generation is defined as the electrons go out from the computational domain as:

3. Primary RE generation rate

$$\frac{dn_{rp}}{dt} = \int \nabla \cdot S d\mathbf{p}, \quad (p_{max}^2/m \sim 1\text{MeV})$$

- Secondary RE generation rate is expressed as a function of RE density n_r and E/E_C :

4. Secondary RE generation rate

$$\frac{dn_{rs}}{dt} = S_{avalanche}(n_r, E/E_C)$$

- $E_C = E_D(v_{th}/c)^2$

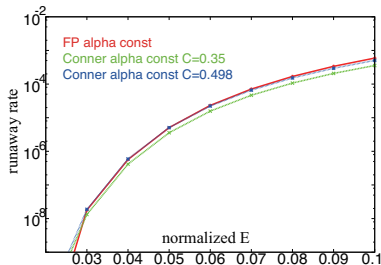
Benchmark: primary RE gen. rate

- In order to confirm the influence of the hot-tail effect, we implement the other primary RE generation rate derived by Conner and Hastie (1975) which do not consider the hot-tail effect.

3-2. Primary RE generation rate without hot-tail effect

$$\frac{dn_{rp}}{dt} = S_{dreicer}(E/E_D, T)$$

- Under the condition of the steady electric field and constant background temperature, the values of these primary RE gen. rate have good agreement.



Parameters (JT-60U like)

■ Initial profiles (impurity species: C)

$$\begin{aligned}R &= 3.4\text{m}, \kappa = 1.6, a = \sqrt{\kappa} \times 1\text{m} \\n_e(\rho) &= (0.4 - 0.04)(1 - \rho^2)^{2/3} + 0.04 \quad [\times 10^{20}] \\T(\rho) &= (2.0 - 0.2)(1 - \rho^2)^2 + 0.2 \quad [\text{keV}] \\j(\rho) &= j_0(1 - \rho^{1.74})^{3.23} \\n_D(\rho) &= (0.24 - 0.024)(1 - \rho^2)^{2/3} + 0.024 \quad [\times 10^{20}] \\Z_{eff} &= 3, I_{init} = 1.052\text{MA}\end{aligned}$$

■ Thermal quench model

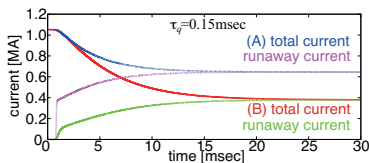
$$\begin{aligned}T(t, \rho) &= (T(0, \rho) - T_f(\rho)) * \exp(-t/\tau_q) + T_f(\rho) \\T_f(\rho) &= T_f(0)(1 - 0.9\rho^2)\end{aligned}$$

■ τ_q : thermal quench time, $T_f(0) = 10\text{eV}$: post-quench temperature

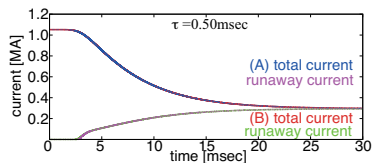
1) Evolutions of current

■ Time evolution of the net plasma current and RE current

■ (A): with hot-tail, (B): without hot-tail



$\tau_q = 0.15 \text{ msec}$

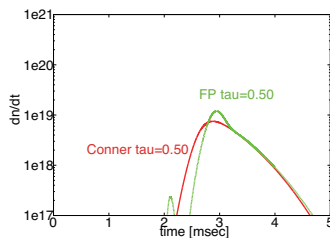
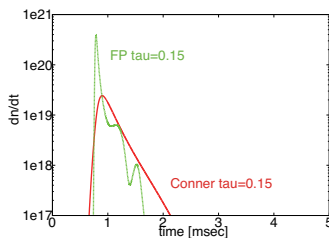


$\tau_q = 0.50 \text{ msec}$

- The RE current increase due to the hot-tail effect.
- The differences between A and B becomes larger as the thermal quench time becomes shorter.

2) Evolutions of dn/dt

- Time evolution of dn_{rp}/dt
- Focus on $0 < t < 5\text{msec}$: primary REs are generated mainly

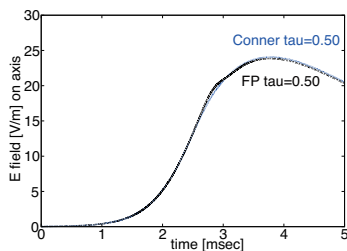
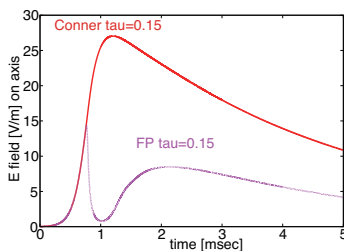


- For faster thermal quench case ($\tau_q = 0.15\text{msec}$), the hot-tail effect enhances the peak value of dn_{rp}/dt and the duration of RE gen. decreases.
- For slower thermal quench case, the hot-tail effect is not remarkable.

3) Evolutions of E

- Time evolutions of E_{\parallel} on axis

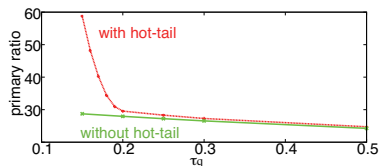
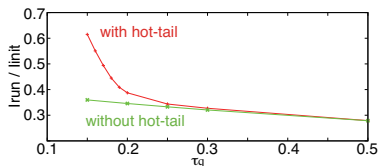
- (L): $\tau_q = 0.15\text{msec}$, (R): $\tau_q = 0.50\text{msec}$



- The strong peak of dn_{rp}/dt reduces E_{\parallel} for $\tau_q = 0.15\text{msec}$
- For the slow quench case, the hot-tail effect is also not remarkable to E_{\parallel} .

4) hot-tail formation

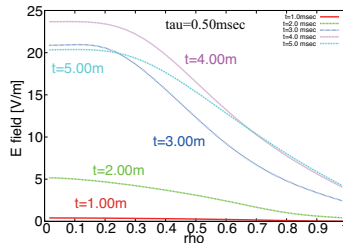
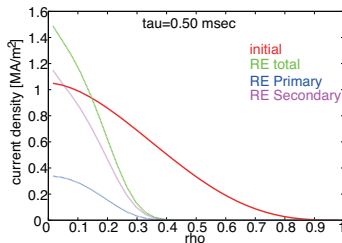
- (L): relation between I_{run}/I_{init} and τ_q
- (R): primary RE current ratio (I_{prim}/I_{run}) v.s. τ_q



- The hot-tail effect is notable for $\tau_q < 0.25\text{msec}$
 - If the thermal quench time is longer than the e-e slowing down time of almost all electrons, it is presumed that the tail of f is not formed.
 - $\tau_{ee}^s(v) = 2\pi\epsilon_0^2 m^2 v^3 / n_e q^4 \ln \Lambda$
 - $\tau_{ee}^s(3v_{th0}) \sim 0.26\text{msec}$ in this case.
 - Since the most of electrons have the velocity $0 < v < 3v_{th0}$, the hot-tail effect is not effective for $\tau_q > 0.25\text{msec}$.

4) radial profiles-1

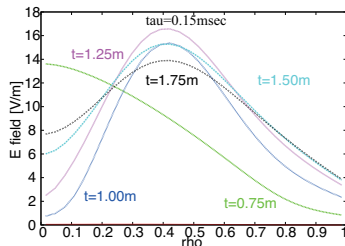
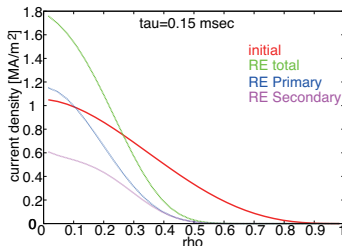
- (L): current density profile ($\tau_q = 0.50\text{msec}$)
- (R): electric field profile ($\tau_q = 0.50\text{msec}$)



- RE current density profile is peaked on axis.
 - $n_{rp}/n_r = 0.247$ (FP)
 - $n_{rp}/n_r = 0.242$ (Conner)
- E has flat profiles during disruption on axis.

5) radial profiles-2

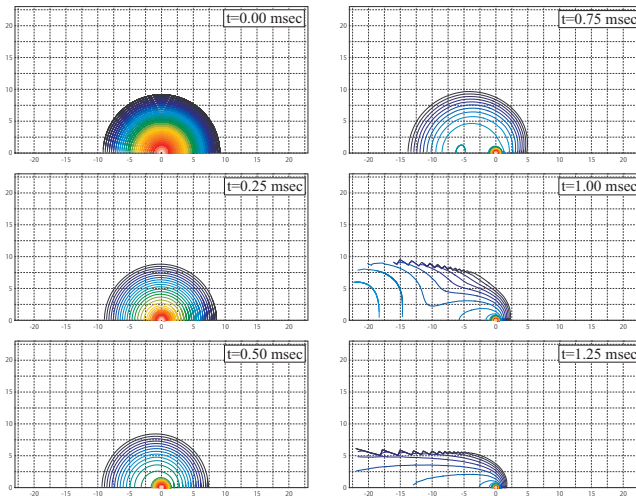
- (L): current density profile ($\tau_q = 0.15\text{msec}$)
- (R): electric field profile ($\tau_q = 0.15\text{msec}$)



- Faster thermal quench enhances the primary ratio
 - $n_{rp}/n_r = 0.588$ (FP)
 - $n_{rp}/n_r = 0.287$ (Conner)
- Due to the high primary RE gen. rate on axis, E has hollow profiles.

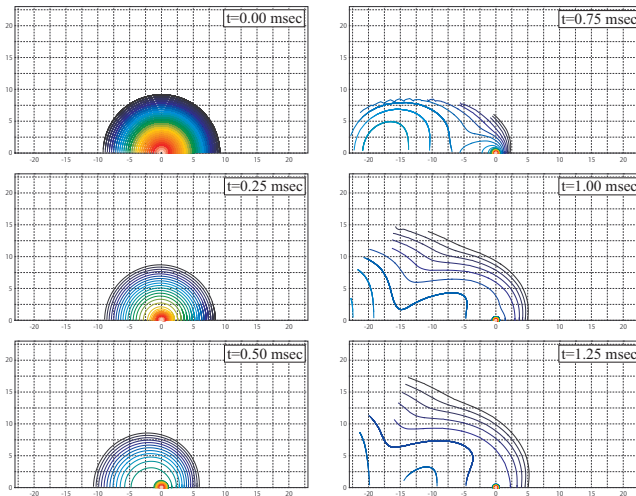
6) f in 2D momentum space-1

- The evolution of the momentum distribution function ($\tau_q = 0.20$)



7) f in 2D momentum space-2

- The evolution of the momentum distribution function ($\tau_q = 0.15$)



Summary

- RE generation including hot-tail effect were simulated.
 - If the temperature drops quickly enough, the hot-tail effect becomes remarkable.
 - In the relatively-slow thermal quench cases, $\tau_q > 0.25\text{msec}$, Fokker-Planck primary RE gen. rate returns similar results to that of analytical one.
 - It seems that thermal quench time affects the pitch angle of REs.
 - The threshold value of τ_q which affects hot-tail effect can be estimated from the slowing down time τ_s