

Development of L-H Transition Simulation Framework with BOUT++ code

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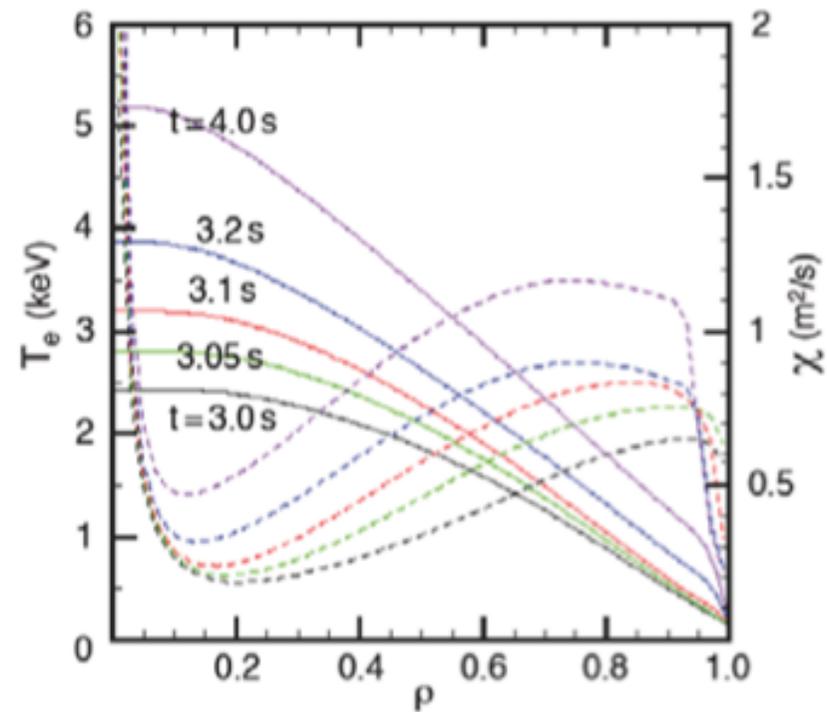
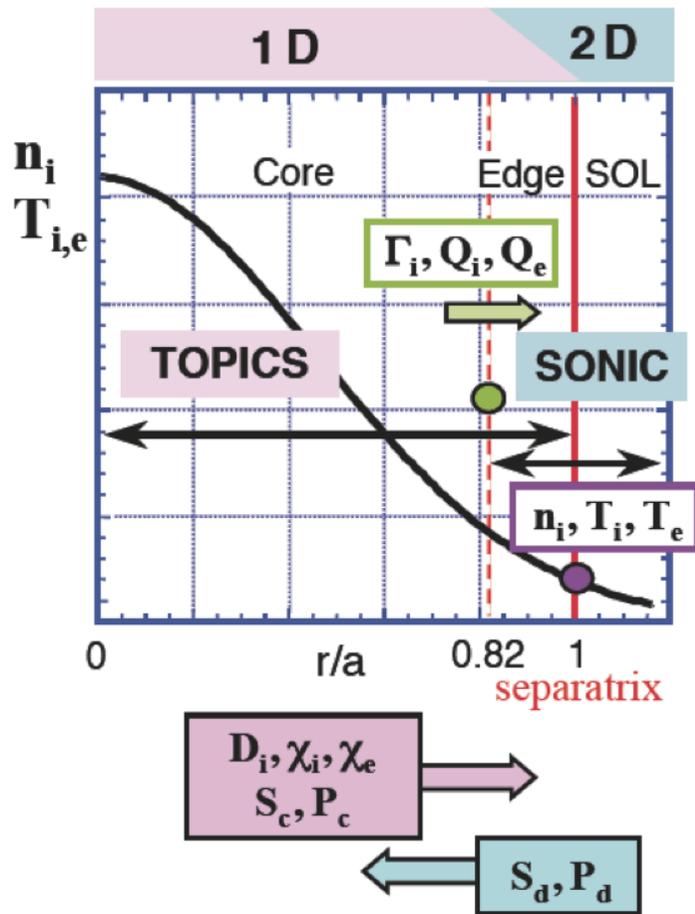


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Motivation for L-H transition simulation by RMHD model

- **Understanding of L-H transition mechanism is one of key issues for**
 - designing a high performance core plasma
 - controlling the heat load on plasma facing materials
- **Integrated transport simulation framework for L-H transition in JAEA^[1]**
 - 1.5D core transport code **TOPICS** + 2D SOL/divertor transport code **SONIC**
 - **CDBM turbulent transport model**
 - **Qualitative evaluation** was accomplished in this framework
 - **Spontaneous turbulence quench at edge region by mean flow shear**
 - **Quantitative evaluations** of L-H transition were not accomplished in this framework
 - **Pressure at pedestal top**
 - **Power threshold for L-H transition**

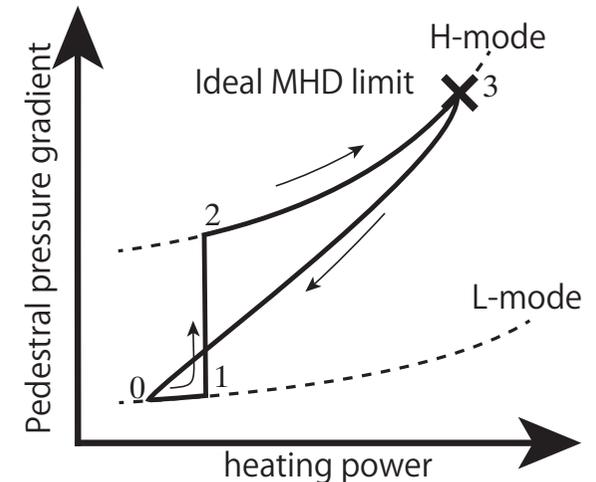


(left): concept of integrated transport simulation framework by TOPICS + SONIC
 (right): time evolutions of T_e and χ

Improvement of turbulent transport model or development of first principal simulation framework are required for quantitative analysis of L-H transition.

- **Improvement of LH transition simulation frameworks through comparison with first principal and integrated transport simulations**
 - **From first principal simulation to integrated transport simulation**

- Improvement of CDBM turbulent transport model by introducing
 - **turbulence suppression by zonal flow shear**
 - **contribution from SOL/divertor transport**
- **From integrated transport simulation to first principal simulation**
 - Improvement of SOL/Divertor physics model in BOUT++ by
 - **Implementation of neutral particle/impurity transport model**
 - **Improvement of sink model**
- **Framework for whole-time edge plasma simulation**
 - **LH transition (1-2): BOUT++**
 - **Pedestal formation (2-3): TOPICS/SONIC**
 - **ELM collapse (3-0): BOUT++**



In this study we have been developing L-H transition simulation framework with CDBM turbulence based on 3-D nonlinear edge MHD/turbulence code BOUT++

Minimal set for L-H transition simulation by RMHD model

- **3D flux-driven simulations of L-H transition by 2-field RMHD model**^[2,3]
 - Resistive ballooning mode turbulence
 - Sheared mean flow by poloidal damping
 - Self-consistent pressure evolution by dynamic heat balance

$$\frac{\partial U_E}{\partial t} = -[\phi, U_E] - B^2 \nabla_{\parallel} J_{\parallel} + \mathbf{b}_0 \times \boldsymbol{\kappa} \cdot \nabla P + \mu_{\perp} \nabla_{\perp}^2 U_E - \mu_{nc} [\bar{U}_E - \delta(k_{nc} - 1)\bar{U}_D]$$

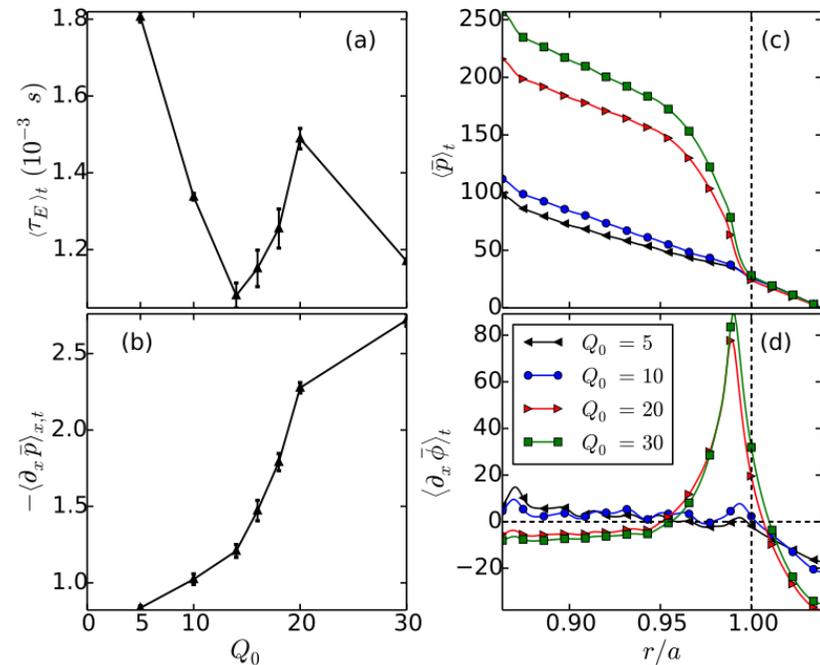
$$\frac{\partial P}{\partial t} = -[\phi, P] + \chi_{\parallel} \nabla_{\parallel}^2 P + \chi_{\perp} \nabla_{\perp}^2 P + S_p - L_p$$

$U_E = \nabla_{\perp}^2 \phi$, $U_D = \nabla_{\perp}^2 P$, $J = S \nabla_{\parallel} \phi$,
 $\delta = d_i/4B_0$, d_a : skin depth, $P_i = P_e = P/2$,
 $[f, g] = \mathbf{b} \times \nabla_{\perp} f \cdot \nabla_{\perp} g$, \bar{f} : (0,0)-component
of f , S_p : heat source, L_p : heat sink,
 μ_{nc} , k_{nc} : quantities related to neoclassical
flow/friction coefficients, $n_i = \text{const.}$

Red term describes poloidal damping

[2] L. Chône *et al.* Phys. Plasmas **21**, 070702 (2014)

[3] G.Y. Park *et al.*, IAEA-FEC 2014 TH-8-1



L-H transition simulation by L. Chône [2]

Derivation of poloidal damping term

length	$L_N = R_{\text{mag}}$	vorticity	$U_N = 1/t_N$
magnetic field	$B_N = B_{\text{mag}}$	vector potential(ish)	$\psi_N = L_N$
velocity	$V_N = V_{AN} = B_N / \sqrt{\mu_0 m_i n_i}$	electrostatic potential	$\phi_N = V_N L_N B_0$
time	$t_N = L_N / V_N$	resistivity	$\eta_N = \mu_0 V_N L_N$
viscosity	$\mu_N = L_N^2 / t_N$	hyper-resistivity	$\lambda_N = \mu_0 \bar{V}_A L_N^3$
pressure	$P_N = B_N^2 / 2\mu_0$	diffusivity	$\chi_N = L_N^2 / t_N$
current	$J_N = -B_0 / \mu_0 L_N$	viscosity	$\mu_N = L_N^2 / t_N$
frequency	$\nu_N = t_N^{-1}$	heat source & sink	$W_N = P_N / t_N$

- **Poloidal damping term is derived from**

- Gianakon's heuristic closure for parallel viscous force^[3]
- Radial force balance with poloidal rotation of ion
- Parallel force balance of ion in neoclassical transport theory^[4]

- **Gianakon's heuristic closure for parallel viscous force in SI unit**

$$\nabla \cdot \overleftrightarrow{\Pi}_{i\parallel} = m_i n_i (\langle B^2 \rangle / B_\theta^2) (\mu_{i1} \bar{V}_{i\theta} + \mu_{i2} \bar{W}_{i\theta}) \mathbf{e}_\theta, \quad \mathbf{W}_i = 2\mathbf{q}_i / 5P_i \quad (1)$$

$$\mathbf{B} = \nabla\zeta \times \nabla\psi + B_\zeta \nabla\zeta, \quad \mathbf{e}_\theta = \sqrt{g} \nabla\zeta \times \nabla\psi, \quad g^{\psi\zeta} = g^{\theta\zeta} = 0, \quad g^{\zeta\zeta} = R^{-2}$$

- (ψ, θ, ζ) is the orthogonal toroidal coordinates
- Red colored term is additional term expressing contribution from heat flux
- Contribution from heat flux results in offset poloidal flow term

- **Ion poloidal flow by radial force balance w/ poloidal rotation**

$$\nabla \bar{P}_i \cdot \nabla \psi = e_i n_i (-\nabla \bar{\phi} + \bar{\mathbf{V}}_i \times \mathbf{B}) \cdot \nabla \psi$$

$$\bar{V}_{i\theta} = \frac{\sqrt{g} g^{\psi\psi}}{B_\zeta} \frac{d}{d\psi} \left(\bar{\phi} + \frac{\bar{P}_i}{e_i n_i} \right), \quad \frac{\langle B^2 \rangle}{B_\theta^2} \bar{V}_{i\theta} \mathbf{e}_\theta = \frac{B_0}{B_p^2} \mathbf{b}_0 \times \nabla \left(\bar{\phi} + \frac{\bar{P}_i}{e_i n_i} \right) \quad (2)$$

- **Ion poloidal heat flow determined by parallel force balance in $\varepsilon \ll 1$ limit**

$$\hat{\mu}_{i1} \hat{V}_i^\theta + \hat{\mu}_{i2} \hat{W}_i^\theta = 0, \quad \varepsilon = \frac{r}{R}, \quad \hat{f}_i^\theta(\psi) = \frac{f^\theta}{B^\theta}, \quad \hat{\mu}_{ij} = \frac{3 \langle (\nabla_{\parallel} B)^2 \rangle}{\langle B^2 \rangle} \mu_{ij}$$

$$\hat{\mu}_{i2} \hat{V}_{i\theta} + \hat{\mu}_{i3} \hat{W}_{i\theta} = l_{22}^{ii} \left(\frac{\bar{V}_{2i} B}{\langle B^2 \rangle} + \hat{W}_i \right), \quad l_{22}^{ii} \gg \hat{\mu}_{ij}, \quad \bar{V}_{2i} = -\frac{B_\zeta}{e_i B} \frac{d\bar{T}_i}{d\psi}, \quad \bar{V}_{i\theta} = -\frac{\mu_{i2}}{\mu_{i1}} \bar{W}_{i\theta}$$

$$\bar{W}_{i\theta} = \frac{\sqrt{g} g^{\psi\psi}}{B_\zeta} \frac{d}{d\psi} \left(\frac{\bar{P}_i}{e_i n_i} \right), \quad \frac{\langle B^2 \rangle}{B_\theta^2} \bar{W}_{i\theta} \mathbf{e}_\theta = \frac{B_0}{B_p^2} \mathbf{b}_0 \times \nabla \left(\frac{\bar{P}_i}{e_i n_i} \right) \quad (3)$$

- **From (1)-(3), Gianakon's heuristic closure becomes**

$$\nabla \cdot \overleftrightarrow{\Pi}_{i\parallel} = m_i n_i \mu_{i1} \frac{B_0}{B_p^2} \mathbf{b}_0 \times \nabla \psi \left[\frac{d}{d\psi} \left(\bar{\phi} + \frac{\bar{P}_i}{e_i n_i} \right) - k_{nc} \frac{d}{d\psi} \left(\frac{\bar{P}_i}{e_i n_i} \right) \right]$$

Red terms describes radial force balance with neoclassical poloidal flow

- Interpolation formula for μ_{i1} and k_{nc}

$$\mu_{i1} = \frac{0.66\varepsilon^{1/2}\nu_i}{(1 + 1.03\nu_{i*}^{1/2} + 0.31\nu_{i*})(1 + 0.66\varepsilon^{3/2}\nu_{i*})}$$

$$k_{nc} = \frac{1}{1 + \nu_{i*}^2 \varepsilon^3} \left(\frac{1.17 - 0.35\nu_{i*}^{1/2}}{1 + 0.7\nu_{i*}^{1/2}} - 2.1\nu_{i*}^2 \varepsilon^3 \right)$$

- Gianakon's heuristic closure results in poloidal damping term

$$\mathbf{b} \cdot \nabla \times \nabla \cdot \overleftrightarrow{\Pi}_{i\parallel} = m_i n_i \mu_{nc} \left[\nabla_{\perp}^2 \frac{\bar{\phi}}{B_0} - (k_{nc} - 1) \nabla_{\perp}^2 \frac{\bar{P}_i}{e_i n_i B_0} \right], \quad \mu_{nc} = \mu_{i1} \frac{B_0^2}{B_p^2}$$

$$\xrightarrow{\text{normalize}} \mu_{nc} [\bar{U}_E - \delta(k_{nc} - 1)\bar{U}_D],$$

- with self-consistently evolving coefficients $\mu_{nc}(\nu_{i*}) \rightarrow \mu_{nc}(P)$, $k_{nc}(\nu_{i*}) \rightarrow k_{nc}(P)$

[4] T.A. Gianakon et al., Phys. Plasmas 9, 536 (2002)

[5] S.P Hirshman and D.J. Sigmar, Nucl. Fusion 21, 1079 (1981)

Preliminary simulations by simplified 2-field model by BOUT++

- **Simplified 2-field RMHD model for LH transition**

$$\frac{\partial U_E}{\partial t} = - [\phi, U_E] - B_0^2 \nabla_{\parallel} J_{\parallel} + \mathbf{b}_0 \times \boldsymbol{\kappa} \cdot \nabla P + \mu_{\perp} \nabla_{\perp}^2 U - \mu_{\text{nc}}^* [\bar{U}_E - \delta k_{\text{nc}}^* \bar{U}_D]$$
$$\frac{\partial P}{\partial t} = - [\phi, P] + \chi_{\perp} \nabla_{\perp}^2 P + \chi_{\parallel} \nabla_{\parallel}^2 P + S_p - PL_p$$

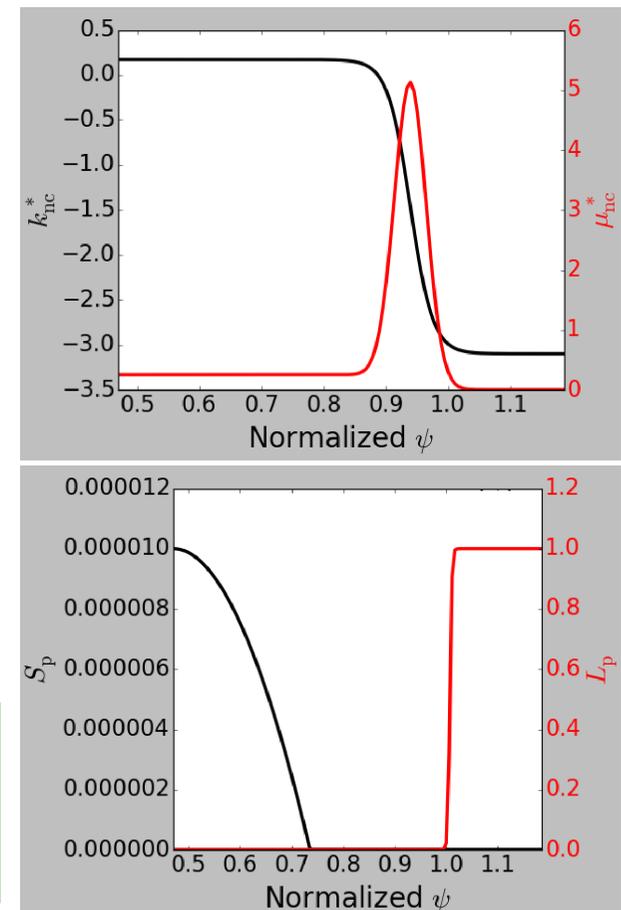
$$\eta = \mu_{\perp} = \chi_{\perp} = 10^{-6}, \quad \chi_{\parallel} = 10^{-2}$$

- **Simplified poloidal damping coefficients**

- Profiles of μ_{nc}^* and k_{nc}^* are given by hyperbolic functions by reference to Ref. [2,3]
- Interaction between E_r shear and diamag. flow through μ_{nc} and k_{nc} are neglected

- **Parabolic heat source and step heat sink**

We have investigated impact of poloidal damping on RMB turbulence



- **Computational grid generated by circular equilibrium generator of BOUT++**

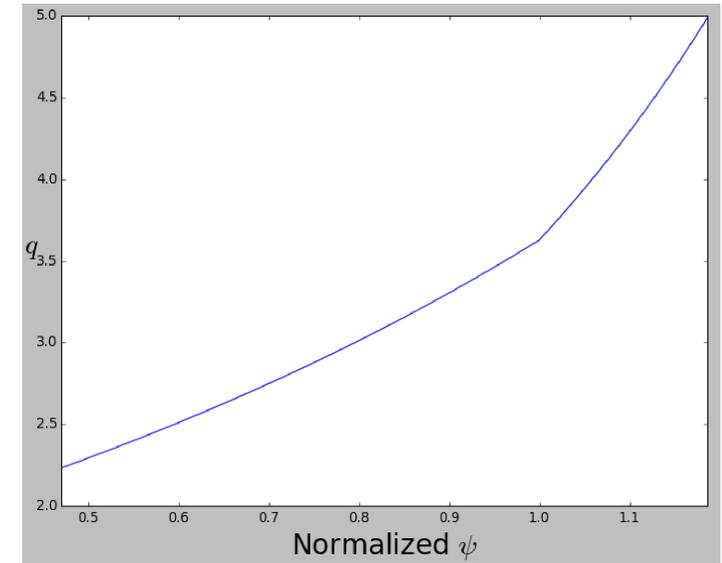
- **Input parameters**

$$R_0 = 300[\text{cm}], \quad a_0 = 75[\text{cm}], \quad B_0 = 4[\text{T}],$$

$$\beta_p = 0.01, \quad \Delta = 5[\text{cm}], \quad n_i = 1.0 \times 10^{19}[\text{m}^{-3}]$$

$$q(\rho) = 1.5 + 2\rho^2, \quad \rho = r/a_0$$

$$p_1(\rho) = 0.5 \left(1 - \tanh \left[\frac{(\rho - 0.4)}{0.225} \right] \right)$$



- **Computational domain:**

$$\text{radial: } 0.47 \leq \psi \leq 1.19, \quad \text{poloidal: } 0 \leq \theta \leq 2\pi, \quad \text{toroidal: } 0 \leq \zeta \leq 2\pi/6$$

- **Resolution:**

$$\text{radial} \times \text{poloidal} \times \text{toroidal} = 132 \times 128 \times 65$$

- **Positions of radial boundary:**

Core boundary: radial index = 0, $\rho = 0.6$, $\psi = 0.47$

Separatrix: radial index = 98, $\rho = 1.0$, $\psi = 1.0$

SOL boundary: radial index = 132, $\rho \simeq 1.2$, $\psi = 1.19$

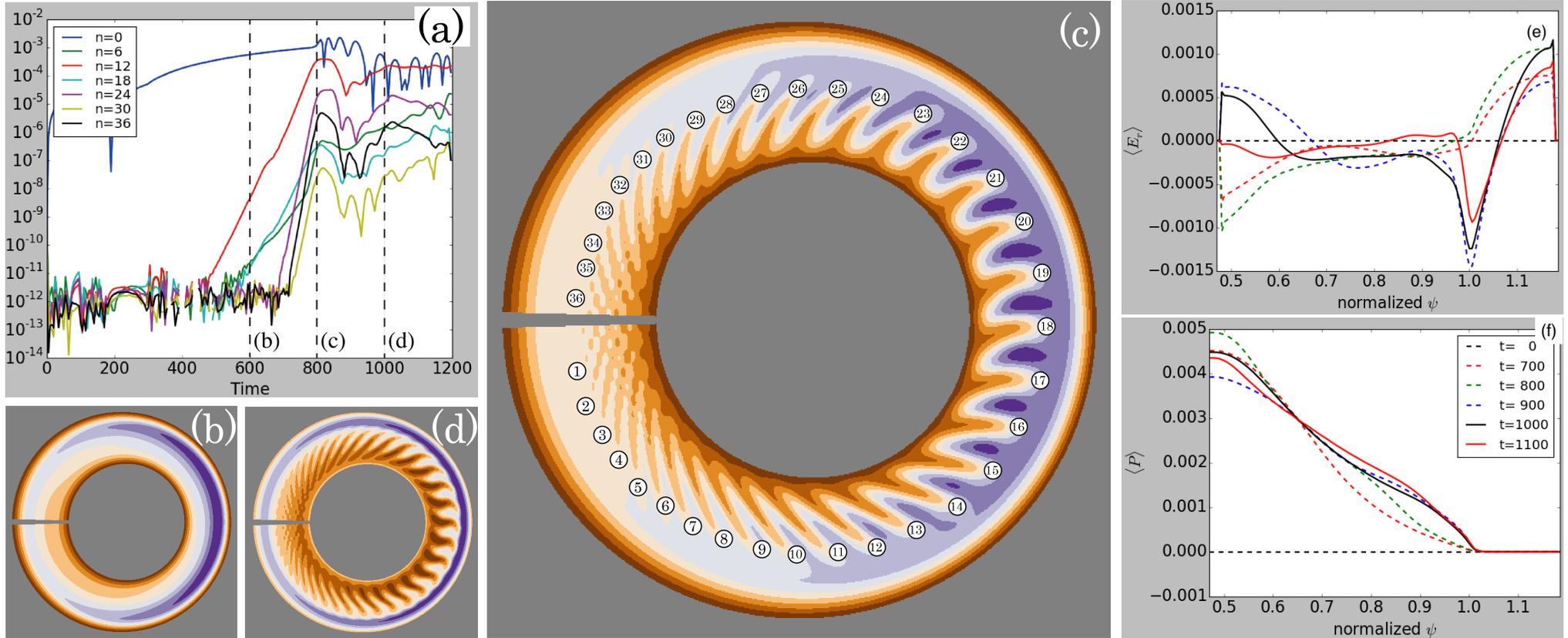
- **Boundary conditions**

$$\frac{\partial U_E}{\partial \psi} = 0, \quad \frac{\partial \phi}{\partial \psi} = 0, \quad \frac{\partial P}{\partial \psi} = 0 \quad \text{at core boundary}$$

$$U_E = 0, \quad \phi = 0, \quad P = 0 \quad \text{at SOL boundary}$$

- **Simulation results of w/ poloidal damping case**

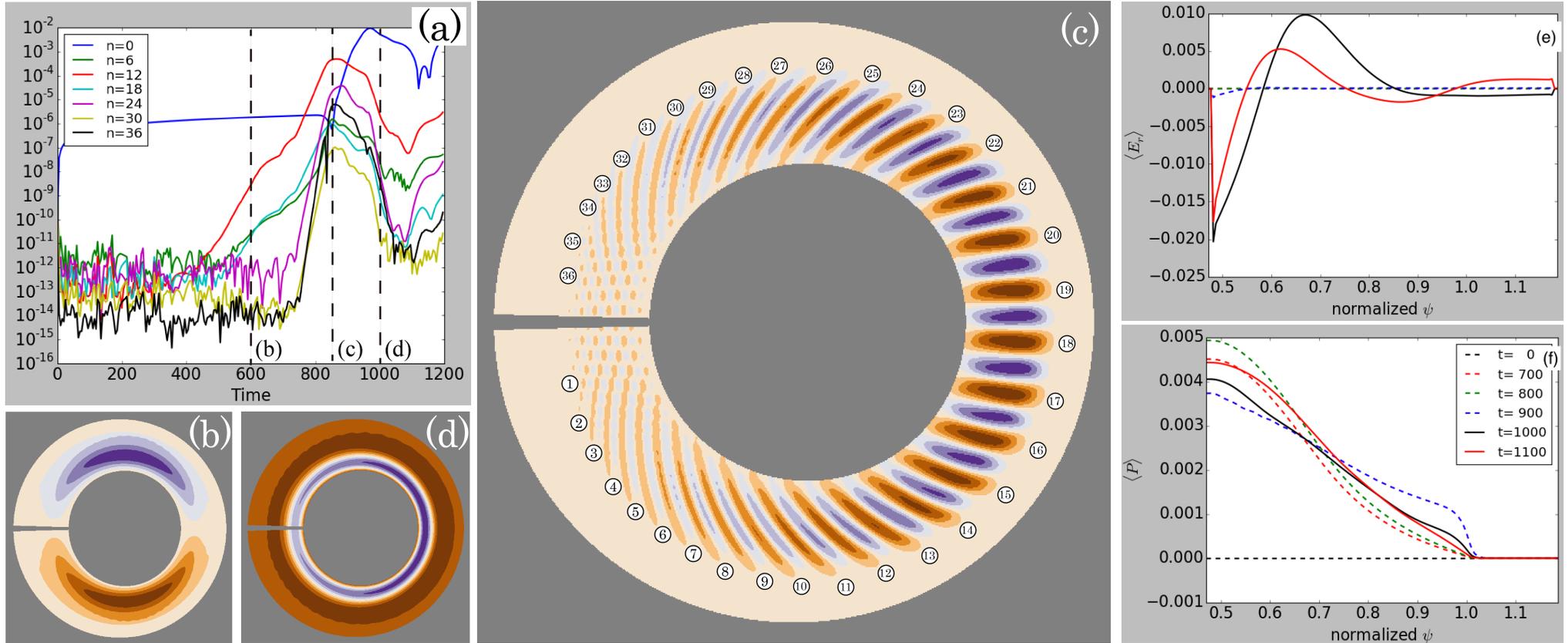
- toroidal mode structure at $\psi \simeq 0.76$ on outer mid-plane (a)
- poloidal plot on $\zeta = 0$ plane at $t = 600\tau_A$ (b), $t = 800\tau_A$ (c), $t = 1000\tau_A$ (d)
- time evolution of flux surface averaged E_r (e) and and P (f)



- * **RBM structure $m = 36$ ($q = 3, n = 12$) was observed at $t = 800\tau_A$**
- * **Strongly sheared E_r was observed at the vicinity of separatrix**
- * **Pedestal-like P profile was obtained**

- **Simulation results of w/o poloidal damping case**

- toroidal mode structure at $\psi \simeq 0.76$ on outer mid-plane (a)
- poloidal plot on $\zeta = 0$ plane at $t = 600\tau_A$ (b), $t = 850\tau_A$ (c), $t = 1000\tau_A$ (d)
- time evolution of flux surface averaged E_r (e) and and P (f)



- * **RBM structure $m = 36$ ($q = 3, n = 12$) was observed at $t = 850\tau_A$**
- * **After $t \simeq 850\tau_A$, simulation was broken and unphysical results are obtained. Improvement of simulation settings is required**

Summary and conclusions

- **Summary**

- **The detailed derivation of poloidal damping term was described**
 - NC poloidal damping term was derived from
 - Gianakon's closure for parallel viscous force
 - Radial force balance with poloidal flow of ion
 - Parallel force balance of ion in neoclassical transport theory
- **Preliminary simulations by 2-field RMHD model + simplified poloidal damping + dynamic heat balance were demonstrated by BOUT++**
 - RBM were observed in both w/ and w/o NC poloidal damping term
 - Poloidal damping generated strongly sheared radial electric field and pedestal-like pressure in the vicinity of the separatrix

- **Future work**

- **Development of postscripts for turbulence analysis**
- **Implementation of self-consistent μ_{nc} and k_{nc}**
- **LH transition simulation by 3-field RMHD model**

(extra) L-H transition simulation framework by 3-field RMHD

- **3-field RMHD model for L-H transition with CDBM turbulence**

$$\frac{\partial \Psi}{\partial t} = - [\phi, \Psi] - \frac{1}{B_0} \nabla_{\parallel}^0 (B_0 \phi) + d_i^* \nabla_{\parallel} P + \eta J_{\parallel} - \lambda \nabla_{\perp}^2 J_{\parallel}$$

$$\begin{aligned} \frac{\partial U}{\partial t} = & - [\varphi, U] + \frac{d_i^*}{2} ([P, U] + [\varphi, U_D] + \nabla_{\perp}^2 [P, \varphi]) \\ & - B_0^2 \nabla_{\parallel} J_{\parallel} + \mathbf{b}_0 \times \boldsymbol{\kappa} \cdot \nabla P + \mu_{\perp} \nabla_{\perp}^2 U - \mu_{\text{nc}} [\bar{U}_E - \delta(k_{\text{nc}} - 1) \bar{U}_D] \end{aligned}$$

$$\frac{\partial P}{\partial t} = - [\phi, P] + \chi_{\perp} \nabla_{\perp}^2 P + \chi_{\parallel} \nabla_{\parallel}^2 P + S_p - L_p$$

$$\Psi = \psi - d_e^2 J_{\parallel}, \quad \varphi = \phi + d_i^* P, \quad U = \nabla_{\perp}^2 \varphi, \quad J_{\parallel} = \nabla_{\perp}^2 \psi, \quad d_i^* = d_i / 4B_0$$

- **CDBM turbulence + poloidal damping + dynamic heat balance**
- **2-field RMHD model for L-H transition is reproduced if**
 - Two-fluid effects are neglected ($d_e, d_i^* \rightarrow 0$)
 - Electrostatic turbulence is assumed, ($J_{\parallel} = \eta^{-1} \nabla_{\parallel} \phi$)